

EXERCISE - 1 [A]

1. (a)
Isochoric process is constant volume process
2. (b)
When ice and water are in equilibrium $\Delta T = 0$. So molar heat capacity is ∞ .
3. (c)
 $w = -2.303nRT \log \frac{V_2}{V_1}$ (for isothermal process)
So $w_{\text{by gas}} = 2.303nRT \ln \frac{V_1}{V_2}$
4. (b)
 $w = nC_v(T_2 - T_1)$ (for adiabatic process)
So $w_{\text{by gas}} = \frac{nR(T_1 - T_2)}{\gamma - 1}$
5. (A)
For expansion against vacuum $p_{\text{ext}} = 0$
 $\Rightarrow w = -p_{\text{ext}}(V_f - V_i) = 0$
6. (b)
 $W = -2 \times (3.4) = -6.8 \text{ L atm} = -689 \text{ J}$
 $Q = +400 \text{ J}$
 $\Delta U = Q + W = -289 \text{ J}$
7. (c)
 $T_f V_f^{\gamma-1} = T_i V_i^{\gamma-1}$
 $(4T_i) \left(\frac{V_i}{32} \right)^{\gamma-1} = T_i V_i^{\gamma-1}$
 $4 = 32^{\gamma-1}$
 $2^2 = 2^{5(\gamma-1)}$
 $\gamma - 1 = \frac{2}{5} \Rightarrow \gamma = \frac{7}{5} \Rightarrow \text{diatomic}$
8. (a)
For irreversible adiabatic process
 $nC_v(T_f - T_i) = -P_{\text{ext}}(V_f - V_i)$
 $\frac{P_f V_f - P_i V_i}{\gamma - 1} = -P_{\text{ext}}(V_f - V_i)$

$$\frac{1 \times V_f - 10 \times 10}{\frac{2}{3}} = -1(V_f - 10)$$

$$V_f - 100 = -\frac{2}{3}V_f + \frac{20}{3}$$

$$\frac{5}{3}V_f = \frac{320}{3} \Rightarrow V_f = 64L$$

$$T_f = \frac{1 \times 64}{10 \times 10} \times 273 = 174.72 K$$

9. (d)
 $TV^{\gamma-1} = k$
 $T = kV^{1-\gamma}$
 $\ln T = \ln k + (1-\gamma)\ln V$

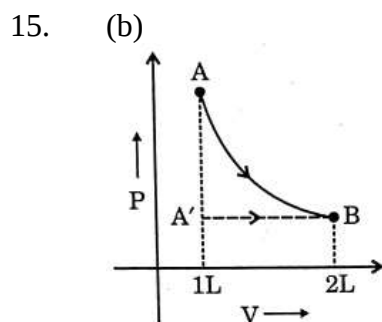
10. (b)
 $Q = 0$, $W = -ve$ (Since expansion)
 So $\Delta U = -ve$

11. (a)
 $W_1 = +15J$ $\Delta U_1 = +30J$
 So $Q_1 = +15J$
 $W_2 = 0$; $\Delta U_2 = -20J$
 So $Q_2 = -20J$

12. (a)
 $Q = +50$, $W = -30$
 $\Delta U = Q + W = +20$

13. (a)
 $T_1 V_1^{\gamma-1} = T_2 V_2^{\gamma-1}$; $\gamma = \frac{5}{3}$; $T_1 = 300K$, $V_1 = 8L$, $T_2 = 250K$
 $V_2 = 8 \times \left(\frac{300}{250}\right)^{\frac{1}{\gamma-1}} = 10.5L$

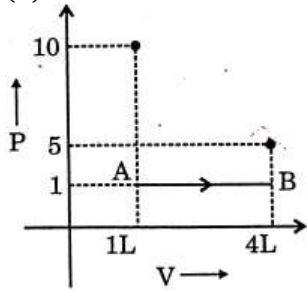
14. (b)
 $P_{\text{ext}} = 0 \Rightarrow w = 0$, $q = 0 \Rightarrow \Delta U = 0$ and $T = \text{constant}$



Final temperature in irreversible is more than reversible as w_{irrev} is less in magnitude.

$$\Rightarrow \Delta H_{\text{rev}} > \Delta H_{\text{irrev}}$$

16. (b)



$$w = -1 \times 3 \text{ L-atm} = -300 \text{ J}$$

$$\frac{10 \times 1}{300} = \frac{5 \times 4}{T} \Rightarrow T = 600 \text{ K}$$

$$q = 50 \times 300 = 15000 \text{ J}$$

$$\Rightarrow \Delta U = q + w = 14700 \text{ J}$$

$$\Delta H = \Delta U + \Delta(PV)$$

$$= 147000 + (20 - 10) \times 100 = 15700 \text{ J}$$

17. (c)

$$q_v = x = 5 \times C_v \times 5;$$

$$q_p = \frac{2x}{5} + 2R \times 5 = \frac{2x}{5} + 2 \times 5 \times \frac{2x}{75} = \frac{10x}{15} = \frac{2x}{3} \text{ J}$$

18. (a)

$$T_1 = 600 \text{ K}$$

$$P_1 = 3 \text{ atm}$$

$$V_1 = 200 \text{ R}$$

$$T_2 = 200 \text{ K}$$

$$P_2 = 1 \text{ atm}$$

$$V_2 = 200 \text{ R}$$

Ischoric →

$$T_2 = 200 \text{ K}$$

$$P_2 = 1 \text{ atm}$$

$$V_2 = 200 \text{ R}$$

adiabatic →

$$P_3 = 3 \text{ atm}$$

$$V_3 = 200 \text{ R} \times \left(\frac{1}{3}\right)^{\frac{1}{\gamma}} = 8.48 \text{ L}$$

$$\text{So } w_3 = -3(16.4 - 8.48)$$

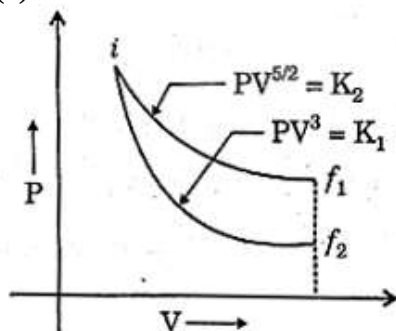
$$= -23.76 \text{ L.atm}$$

19. (a)

E & H depend only on T if n is constant.

$$PdV + VdP = nRdT$$

20. (a)



From the graph, work done in 2nd process is more than 1st process.

21. (d)
In isothermal process, temperature remains constant, while, in adiabatic expansion, temperature ↓ as work is done at the cost of internal energy. T_{final} of rev. adiabatic expansion is least because more work is done in reversible than irreversible adiabatic expansion.
 $\Rightarrow T_a = T_b > T_d > T_c$
22. (d)
$$C_v(\text{mix}) = \frac{1 \times 3R + 2 \times \frac{3}{2}R}{3} = 2R, \Rightarrow C_p = 3R, \gamma = \frac{3}{2}$$
$$T_1 V_1^{\gamma-1} = T_2 V_2^{\gamma-1} \Rightarrow T = \frac{320}{(4)^{0.5}} = 160 \text{ K}$$
$$\Delta U = \frac{-3 \times R \times 160}{\frac{1}{2}} = -960 R$$
23. (b)
 $w = -nR\Delta T = -2 \times 8.314 \times (300 - 400)$
 $= +1662.8 \text{ J}$
24. (c)
Rate can not be predicted by thermodynamics.
25. (c)
$$W = - \int_{10}^{100} \frac{10}{V} dV$$
$$W = \left(-10 \times 2.303 \log \frac{100}{10} \right) \text{ bar-lit}$$
$$W = -23.03 \times 100 = -2303 \text{ J}$$
$$400 = -2303 + q$$
$$q \approx 2700$$
26. (a)
Work = area under the graph = $\pi \times 2 \text{ L} \times 2 \text{ atm} = 4\pi$
27. (a)
 $T_{f, \text{adiabatic}} < T_{f, \text{isothermal}}$
28. (c)
As γ increase graph goes down.
29. (d)
Between same initial & final points there can not be isothermal & adiabatic process.
30. (d)
For formation reaction, reactants should be elements in their most stable allotropic state.
31. (b)
For combustion reaction, substance should be burned with sufficient oxygen.

32. (a)
Kirchoff's equation are

$$\Delta H_2 = \Delta H_1 + \Delta C_p (T_2 - T_1)$$

$$\Delta E_2 = \Delta E_1 + \Delta C_v (T_2 - T_1)$$
33. (c)
 $\Delta H = \Delta E + \Delta n_g (RT)$, Δn_g for the reaction is positive
 So $\Delta H < \Delta E$

34. (a)

$$\Delta H_f^\circ = -\frac{22}{2} = -11 \text{ kcal / mole}$$

35. (a)
Calorific values

$$\text{CH}_4 \rightarrow \frac{890}{16} = 55.625 \text{ kJ / g}$$

$$\text{C}_2\text{H}_4 \Rightarrow \frac{1411}{28} = 50.393 \text{ kJ / g}$$

$$\text{C}_2\text{H}_6 \Rightarrow \frac{1560}{30} = 52 \text{ kJ / g}$$

36. (b)

$$\Delta E = \Delta H - \Delta n_g (RT)$$

$$= 176 - 1 \times \frac{8.314}{1000} \times 1240 = 165.6 \text{ kJ}$$

37. (b)
(ii)- (i)

$$\Delta H = -393.5 + 395 = 1.5 \text{ kJ}$$

38. (a)

$$\text{Energy} = \frac{1560}{2} = 44 \times n_{\text{H}_2\text{O}}$$

$$\Rightarrow n_{\text{H}_2\text{O}} = 17.727$$

$$\Rightarrow w_{\text{H}_2\text{O}} = 319 \text{ g}$$

39. (b)

$$\text{K} + \text{H}_2\text{O} \rightarrow \text{KOH}(\text{aq}) + \frac{1}{2} \text{H}_2 - 48$$

$$\text{H}_2 + \frac{1}{2} \text{O}_2 \rightarrow \text{H}_2\text{O} \quad -68.39$$

$$\text{KOH}(\text{aq}) \rightarrow \text{KOH}(\text{s}) + \text{aq} \quad 14$$

$$\text{K} + \frac{1}{2} \text{O}_2 + \frac{1}{2} \text{H}_2 \rightarrow \text{KOH}(\text{s})$$

$$\Delta H = -48 - 68.39 + 14 = -102.39$$

40. (a)
 $\Delta H - \Delta U = (\Delta n_g)RT$
 $= -3 \times \frac{8.314}{1000} \times 298 =$
 $= -7.43$
41. (a)
 $\Delta H = \Delta E + (\Delta n_g)RT$
 $\Delta H = \Delta E - (5.5) \times \frac{8.314 \times 298}{1000}$
 $C_8H_{18(g)} + \frac{25}{2}O_2(g) \rightarrow 8CO_2(g) + 9H_2(l)$
 $\Delta n_g = 8 - 1 - 12.5 = -5.5$
42. (a)
 It is not a formation or combustion reaction

43. (b)
 $n_{AL} = \frac{250 \times 4.18}{837.8} = 1.247$
 $\Rightarrow n_{Al_2O_3} = \frac{1.247}{2} = 0.624$

44. (a)
 $\Delta_f H_{H_2SO_4} = -298.2 - 98.7 - 130.2 - 287.3$
 $= -814.4$

45. (b)
 $C_2H_4 + 3O_2 \rightarrow 2CO_2 + 2H_2O$
 $n_{C_2H_4} = \frac{6226}{1411}$
 $n_{O_2} = \frac{6226}{1411} \times 3 \Rightarrow V_{O_2} = \frac{6226}{1411} \times 3 \times 22.4L$
 $= 296.5L$

46. (b)
 (i) – (ii)
 $N_2O_4(g) \rightarrow 2NO_2(g)$
 $\Delta H = 16.18 - 2.31 = +ve$
 $\Rightarrow$ endothermic reaction

47. (d)
 $\frac{1}{2}H_2(g) + \frac{1}{2}Br_2(g) \rightarrow HBr(g) \quad \frac{\Delta H_1}{2}$
 $\frac{1}{2}Br_2(l) \rightarrow \frac{1}{2}Br_2(g) \quad \frac{-\Delta H_2}{2}$

 $\frac{1}{2}H_2(g) + \frac{1}{2}Br_2(l) \rightarrow HBr(g) \quad \frac{\Delta H_1 - \Delta H_2}{2}$

48. (b)
 $\Delta H_T < \Delta H_C$
 So $C \rightarrow T$ $\Delta H_R = \Delta H_T - \Delta H_C = -ve$
 $\Rightarrow$ Exothermic
49. (d)
 $= 265 = 4x + 2 \times 3x = -26$
 $10x = -265 + 26 = -239$
 $x = -23.9$
 $3x = -71.7$
50. (b)

$$\begin{array}{c} C + O_2 \rightarrow CO_2 \\ x \text{ mole} \quad x \text{ mole} \end{array}$$

$$\begin{array}{c} C + \frac{1}{2} O_2 \rightarrow CO \\ (1-x) \text{ mole} \quad \left(\frac{1-x}{2}\right) \text{ mole} \end{array}$$

 $94.05x + 26.41(1-x) = 75$
 $67.64x = 75 - 26.41$
 $x = 0.718$
 $m_{O_2} = 32 \times \left(\frac{1}{2} + \frac{x}{2}\right) = 27.49g$
51. (b)
 For $\Delta H = \Delta E \Rightarrow \Delta n_g = 0$
52. (c)
 $C + O_2 \rightarrow CO_2 \quad \Delta H = -390 \text{ (1)}$
 $CO + \frac{1}{2} O_2 \rightarrow CO_2 \quad \Delta H = -278 \text{ (2)}$
 (1) - (2)
 $\Delta H = -390 + 278 = -112$
53. (d)
 For formation reaction, reactants should be in most stable allotropic form
54. (d)
 $\Delta H_n = -\frac{y}{2}$
55. (a)
 $\theta = m \& \Delta T$
 θ is doubled & m is also doubled.
56. (a)
 $\Delta H_{\text{atomisation}} = \frac{104}{2} = 52$
57. (c)
 For maximum heat, acid and base reacting should be maximum.

58. (b)

$$\text{H}_2(\text{g}) + \frac{1}{2}\text{O}_2(\text{g}) \rightarrow \text{H}_2\text{O}(\ell)$$

$$-298 = 433 + \frac{492}{2} - 42 - 2B_{\text{O}-4}$$

$$B_{\text{O}-4} = \frac{1}{2} \left(433 + \frac{492}{2} - 42 + 298 \right)$$

$$= 467.5$$
59. (d)

$$\text{H}_2\text{O}(\ell) \rightarrow \text{H}_2\text{O}(\text{g})$$

$$\Delta H = +9.7 = \Delta_f H_{\text{H}_2\text{O}(\text{g})} - \Delta_f H_{\text{H}_2\text{O}(\ell)}$$

$$\Rightarrow \Delta_f H_{\text{H}_2\text{O}(\text{g})} = -68 + 9.7 = -58.3 \text{ kcal}$$
60. (b)

$$-100 = 600 - 2B_{\text{C}-\text{C}}$$

$$\Rightarrow BE_{\text{C}-\text{C}} = 350$$
61. (b)

$$\Delta H_n = -13700 + (366 \times 0.86) = -13385$$
62. (b)

$$\frac{1}{2}\text{H}_2 + \frac{1}{2}\text{Cl}_2 \rightarrow \text{HCl}$$

$$\Delta H = \frac{435}{2} + \frac{243}{2} - 431 = -92$$
63. (b)

$$\Delta H_n = -13.7 \times 2$$

$$= -27.4 \text{ kcal}$$
64. (d)
 For max heat $n_{\text{H}^+} = n_{\text{OH}^-}$

$$1 \times V_1 = 0.5 \times 2 \times V_2$$

$$\Rightarrow V_1 = V_2$$
65. (d)

$$\text{S} \rightarrow \ell \rightarrow \text{g}$$

$$\Delta H_{\text{fusion}} + \Delta H_{\text{vaporisation}}$$

$$-100 = \frac{x}{2} + \frac{x}{4} - x = -\frac{x}{4}$$
66. (a)

$$-10 = \frac{x}{2} + \frac{x}{4} - x = -\frac{x}{4}$$

$$\Rightarrow x = 400$$

67. (a)

$$\Delta S = \frac{\theta_{\text{rev}}}{T} = \frac{\Delta H_v}{T}$$
68. (a)

$$\Delta S_{\text{sys}} = nR \ln \frac{V_f}{V_i}$$

$$= 1 \times 8.314 \times \ln 10 = 19.15 \text{ J / K - mol}$$
69. (b)

$$\Delta S_{\text{sys}} = nR \ln \frac{V_f}{V_i}$$
70. (b)
 Endothermic $\Rightarrow \Delta H = +\text{ve}$
 $\Rightarrow \Delta S_{\text{sys}} > 0 \Rightarrow \Delta S_{\text{surr}} = -\text{ve}$
71. (c)
 Exothermic $\Rightarrow H = -\text{ve}$
 $\Rightarrow \Delta S_{\text{sys}} < 0 \Rightarrow \Delta S_{\text{surr}} = +\text{ve}$
72. (b)
 $\Delta H > 0 \Rightarrow$ since bond are broken
 $\Delta S > 0 \Rightarrow \Delta n_g > 0$
73. (d)

$$S_{\text{sys}} = 1 \times C_v \ln 2 + 1 \times R \ln \frac{1}{2}$$

$$= (C_{v-R}) \ln 2$$
74. (a)
 Zeroth law is for thermal equilibrium between bodies
75. (d)

$$\Delta S_{\text{surr}} = \frac{64000}{300} = 213$$
76. (a)

$$\Delta S_{\text{Rxn}} = 2 \times 68 - 2 \times 126.6 - 201.2$$

$$= -318.4$$
77. (a)
 At equilibrium $\Delta G = 0$
78. (a)
 For spontaneous $\Delta G < 0$
79. (d)

$$T > \frac{178.3 \times 1000}{160}$$

$$\Rightarrow T > 1114$$

80. (c)

$$T < \frac{49 \times 1000}{40.2}$$

$$\Rightarrow T < 1219\text{K}$$

81. (b)

$$\Delta H_R = 9.7 - 2 \times 90.5$$

$$= -171.3$$

$$\Delta S_R = 304 - 2 \times 210 - 205$$

$$= -321$$

$$\Delta G_R = -171.3 - \frac{298}{1000} \times (-321)$$

$$= -75.64$$

82. (a)

$\Delta n < 0, \Delta S > 0$ always spontaneous

$\Delta H > 0, \Delta S < 0$ never spontaneous

83. (c)

For $\text{C}_2\text{H}_6(\text{g})$, C will be higher

84. (c)

$$T > \frac{85 \times 1000}{1.98}$$

$$\Rightarrow T > 429.3\text{K}$$

85. (d)

$\Delta H^\circ > 0 \Rightarrow$ opposes

$\Delta S > 0 \Rightarrow$ favours

EXERCISE - 1 [B]

1. (d)
 $41 + 463 + 348 - 352 - 415 = 85 \text{ kJ/mol}$
2. (a)

$$\left[n \times 942 + n \times 436 - n \times (163 \times 2 + 2 \times 390) \right] \times \frac{1}{n} = 272 \text{ kJ/mole}$$
3. (b)

$$\Delta H^\circ = -167.1 \times 5 - 1284.4 + 285.8 \times 4 + 443.5$$

$$= -533.2$$
4. (b)

$$\Delta H^\circ = \frac{507}{2} - \frac{427}{2} + \frac{43}{2} + \frac{34}{2} = 78.5 \text{ kJ}$$
5. (c)
6. (c)
7. (a)
8. (b)

$$\Delta H_1 = x + \frac{3}{2} \Delta H_3 - \frac{\Delta H_2}{2}$$

$$\Rightarrow x = \Delta H_1 + \frac{\Delta H_2}{2} - \frac{3}{2} \Delta H_3$$
9. (b)

$$\Delta H^\circ = -537 \times 2 - 680 \times 2 + 52 = -2382$$
10. (b)

$$\frac{1}{2} \text{I}_2(s) + \frac{1}{2} \text{Cl}_2(g) \longrightarrow \text{ICl}(g)$$

$$\Delta H_f = \frac{1}{2} \times [62.76 + 151 + 242.3] - 211.3$$

$$= +16.8 \text{ kJ/mol}$$
11. (c)
12. (b)
 $\Delta H - T \Delta S > 0$ (For non-spontaneous process)

$$\Rightarrow T > \frac{-\Delta H}{-\Delta S} \text{ or } T > \frac{1648 \times 10^3}{560} = 2943 \text{ K}$$
13. (d)

14. (b)

15. (b)

16. (b)

$$\begin{array}{cccc} \text{Ice} & \rightarrow & \text{water} & \rightarrow & \text{water} & \rightarrow & \text{steam} \\ (0^\circ\text{C}) & & (0^\circ\text{C}) & & (100^\circ\text{C}) & & (100^\circ\text{C}) \end{array}$$
$$\Delta S_{\text{Total}} = 18 \times \frac{80}{273} + 18 \times 1 \times \ln\left(\frac{373}{273}\right) + 18 \times \frac{540}{373}$$

17. (b)

$$T = \frac{25 \times 10^3}{50} \text{ K}$$

18. (b)

19. (d)

$$\begin{array}{ccc} A(s) & \rightarrow & B(s) \\ 400 \text{ mL} & & 600 \text{ mL} \end{array}$$
$$\int d(\Delta G) = \int (\Delta G) dP$$
$$\Delta G - \Delta G^\circ = (200) [P - 10^5]$$
$$\frac{2 \times 10^3}{200 \times 10^{-6}} = P - 10^5$$
$$\Rightarrow P = 101 \times 10^5 \text{ N/m}^2$$
$$= 101 \text{ bar}$$

20. (a)

$$\Delta S_{\text{sys}} = nC_v \ln\left(\frac{T_2}{T_1}\right) + nR \ln\left(\frac{V_2}{V_1}\right)$$
$$\Delta S = 2 \times \frac{3}{2} \times 2 \ln\left(\frac{10}{10}\right) + 2 \times 2 \ln\left(\frac{5}{10}\right)$$

21. (b)

22. (a)

$$W = -\frac{7}{28} \times 8.3 \times 300 \ln\left(\frac{0.5}{0.1}\right) = -996 \text{ J}$$

23. (b)

$$\Delta E = \Delta H - \Delta n_g RT ; \Delta n_g > 0 \text{ and } \Delta H < 0$$

CO formation is exothermic and $\Delta n_g = +1$

24. (c)

$$q = 0 ; \Delta U = -4(30 - 40) = +40$$

$$\Delta H = \Delta U + \Delta(PV) = 40 + (120 - 80) = 80 \text{ L-bar}$$

$$\Delta H = 8000 \text{ J}$$

25. (d)

$$q = 10 \times 1 \ln 10 = 23.03 \text{ atm-L}$$

EXERCISE - 1 [C]

1. (189)
 $\text{Zn} + 2\text{HCl} \longrightarrow \text{ZnCl}_2 + \text{H}_2(g);$
 $w = -\Delta n_g RT$

$$= -1 \times 8.3 \times 296 \times \frac{5}{65} \simeq -189$$
2. (22)

$$\frac{57.4}{2^{1.4}} = P_2 \quad \Rightarrow \quad P_2 = 22$$
3. (6)
 Open systems : b, f, g, i, j
 Closed systems : a, c, h
 Isolated systems : d, e
4. (5200)

$$W = -\int_1^3 P dV = -\int_1^3 6V^2 dV = 2 \times [27 - 1]$$

$$= 52 \text{ bar-m}^3 \text{ or } 5200 \text{ kJ}$$
5. (182)
 $[23 + 45 + 81 + 33 = 182]$
6. (44)
 $(\Delta C_p)_{\text{Reaction}} = 2 \times 4 - 3.5 - 3 \times 3.5 = -6$
 $\Delta H_{300} = \Delta H_{1000} + \Delta C_p (300 - 1000)$

$$= -123.77 + \frac{6 \times 700 \times 8.3}{1000}$$

 $= -88.91 \text{ for 2 moles of } \text{NH}_3$
7. (5)
 Pressure, molar entropy, density, boiling point, molality are intensive properties.
8. (1488)
 $\Delta_r H^\circ = 2 \times 414 + 2 \times 330 = 1488 \text{ kJ/mol}$
9. (210)
 $P_4(s) \longrightarrow P_4(g)$
 $P_4(s) \longrightarrow 4P(g)$
 $\Rightarrow P_4(g) \longrightarrow 4P(g)$
 $\Delta H = 1321 - 61 = 6x$
 $\Rightarrow x = 210 \text{ kJ/mol}.$

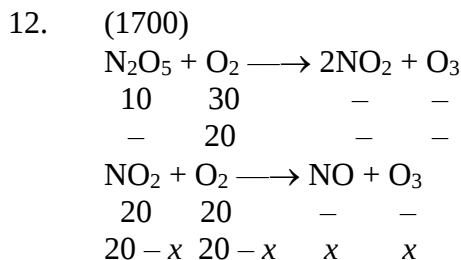
10. (4)
Intensive : a, c, d, f, g, h, i, k
Extensive : b, e, j, l

11. (3125)

$$300 \times (0.5)^{\gamma-1} = T_2 \times (3)^{\gamma-1}$$

$$\Rightarrow T_2 = \frac{300}{(6)^{2/5}} = 150 \text{ K}$$

$$w = 1 \times \frac{25}{3} \times \frac{150}{0.4} = 3125 \text{ J}$$



$$\frac{(10+x)}{[(20-x) + (20-x) + x + (10+x)]} \times 100 = 50$$

$$\Rightarrow x = 15$$

$$\Delta H = 10 \times 200 - 15 \times 20 = 1700 \text{ kJ}$$

13. (2)

$$29 \times 2 - 56 = 2$$

14. (7700)

$$T \propto V^3, \quad T = 300 \text{ K}$$

$$\Rightarrow PV^{-2} = K \quad n = 1 \text{ mole}$$

$$\gamma = \frac{5}{3}$$

$$C = \frac{3R}{2} + \frac{R}{3} = \frac{11R}{6}; T_f = 2400 \text{ K}$$

$$q = 1 \times \frac{11}{6} \times 2 \times 2100 = 7700 \text{ cal}$$

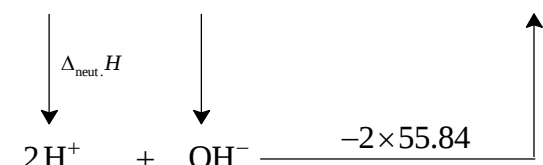
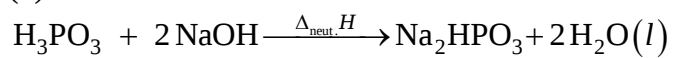
15. (8)

$$\frac{1}{5} = 1 - \frac{T_2}{T_1} \quad \dots(i)$$

$$\frac{2}{5} = 1 - \frac{(T_2 - 80)}{T_1} \quad \dots(ii)$$

$$\Rightarrow T_1 - T_2 = 80$$

16. (5)



$$\Delta_{\text{neut.}}H = \Delta_{\text{ion}}H - 2 \times 55.84$$

$$\Delta_{\text{ion}}H = 5 \text{ kJ}$$

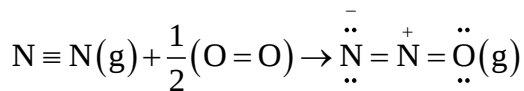
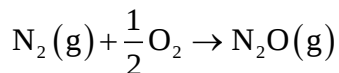
17. (3)

State functions : a, b, c, d, g, h, j

Path functions : e, f, i, k

SECTION-I

1. (a)



$\Delta_f H^\circ = [\text{Energy required for breaking of bonds}] - [\text{Energy released for forming of bonds}]$

$$= \left(\Delta H_{\text{N} \equiv \text{N}} + \frac{1}{2} \Delta H_{\text{O}=\text{O}} \right) - (\Delta H_{\text{N}=\text{N}} + \Delta H_{\text{N}=\text{O}})$$

$$= \left(946 + \frac{1}{2} \times 498 \right) - (418 + 607) = 170 \text{ kJ mol}^{-1}$$

Resonance energy = observed $\Delta_f H^\circ$ – calculated $\Delta_f H^\circ$

$$82 - 170 = -88 \text{ kJ mol}^{-1}.$$

2. (c)

For isothermal reversible expansion.

$$w = -nRT \ln \frac{V_2}{V_1}$$

3. (a)

Process is isothermal reversible expansion, hence $\Delta U = 0$, therefore $q = -w$,

Since $q = +208\text{J}$, $w = -208\text{J}$

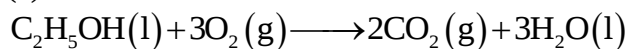
4. (b)

$$\Delta S^\circ = S^\circ_{\text{CO}_2} + 2 \times S^\circ_{\text{H}_2\text{O}} - (S^\circ_{\text{CH}_4} + 2 \times S^\circ_{\text{O}_2})$$

$$= (213.6 + 2 \times 69.9) - (186.2 + 2 \times 205.2)$$

$$= -242.8 \text{ JK}^{-1} \text{ mol}^{-1}$$

5. (a)



Bomb calorimeter gives ΔU of the reaction.

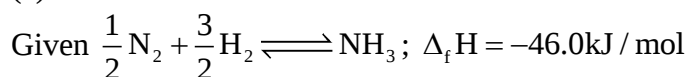
Given, $\Delta U = -1364.47 \text{ kJ mol}^{-1}$

$$\Delta n_g = -1$$

$$\Delta H = \Delta U + \Delta n_g RT$$

$$= -1364.47 - \frac{1 \times 8.314 \times 298}{1000} = -1366.95 \text{ kJ mol}^{-1}$$

6. (c)



$$\Delta_f H(\text{NH}_3) = \frac{1}{2} \Delta H_{\text{N-N}} + \frac{3}{2} \Delta H_{\text{H-H}} - 3 \Delta H_{\text{N-H}} - 46 = \frac{1}{2}(712) + \frac{3}{2}(436) - 3 \Delta H_{\text{N-H}}$$

$$\Delta H_{\text{N-H}} = 352 \text{ kJ/mol}$$

7. (b)

In CH_4 , $4 \times \text{BE}_{(\text{C-H})} = 360 \text{ kJ/mol}$

$$\therefore \text{BE}_{(\text{C-H})} = 90 \text{ kJ/mol}$$

In C_2H_6 , $\text{BE}_{(\text{C-C})} + 6 \times \text{BE}_{(\text{C-H})} = 620 \text{ kJ/mol}$

$$\therefore \text{BE}_{(\text{C-C})} = 620 - (6 \times 90) = 80 \text{ kJ/mol}$$

$$\therefore \text{BE}_{(\text{C-C})} = \frac{80 \times 10^3}{6.023 \times 10^{23}} \text{ J/mol}$$

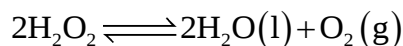
Now, $E = \frac{hc}{\lambda}$

$$\lambda = \frac{6.626 \times 10^{-34} \times 3 \times 10^8 \times 6.023 \times 10^{23}}{80 \times 10^3}$$

$$\lambda = 1.49 \times 10^{-6} \text{ m} \quad (\because 1 \text{ nm} = 10^{-9} \text{ m})$$

$$\therefore \lambda = 1.49 \times 10^3 \text{ nm}$$

8. (a)

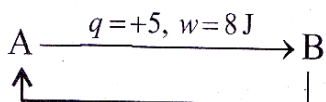


$$w = -P_{\text{ext}}(\Delta V) = -n_{\text{O}_2} RT$$

$\therefore$ 100 mole of H_2O_2 on decomposition give 50 mole O_2 .

$$\therefore w = -(50)(8.3)(300) = -124500 \text{ J} = -124.5 \text{ kJ}$$

9. (d)



$$\Delta U_{AB} = q + w = 5 + (-8) = -3 \text{ J}$$

$$q = -3, \Delta U_{BA} = +3$$

$$\Delta U_{BA} = q + w$$

$$\Rightarrow 3 = -3 + w \Rightarrow w = +6 \text{ (work done on the system).}$$

10. (c)
- $$\text{C}(\text{graphite}) + \text{O}_2(\text{g}) \longrightarrow \text{CO}_2(\text{g}); \Delta_r H_1^\circ = -393.5 \text{ kJ/mol}^{-1} \quad \dots\dots(i)$$
- $$\text{H}_2(\text{g}) + \frac{1}{2} \text{O}_2(\text{g}) \longrightarrow \text{H}_2\text{O}(\text{l}); \Delta_r H_2^\circ = -285.8 \text{ kJ/mol}^{-1} \quad \dots\dots(ii)$$
- $$\text{CO}_2(\text{g}) + 2\text{H}_2\text{O}(\text{l}) \longrightarrow \text{CH}_4(\text{g}) + 2\text{O}_2(\text{g}); \Delta_r H_3^\circ = +890.3 \text{ kJ/mol}^{-1} \quad \dots\dots(iii)$$
- $$\text{C}(\text{graphite}) + 2\text{H}_2(\text{g}) \longrightarrow \text{CH}_4(\text{g}); \Delta_r H = ? \quad \dots\dots(iv)$$
- $$[\text{Eq. (i)} + \text{Eq. (iii)}] + [2 \times \text{Eq. (ii)}] = \text{Eq. (iv)}$$
- $$\therefore [\Delta H_1 + \Delta H_3] + [2 \times \Delta H_2] = \Delta H$$
- $$[(-393.5) + (890.3)] + [2(-285.8)] = -74.8 \text{ kJ/mol}$$
11. (d)
- $$\text{C}_6\text{H}_6(\text{l}) + \frac{15}{2} \text{O}_2(\text{g}) \longrightarrow 6\text{CO}_2(\text{g}) + 3\text{H}_2\text{O}(\text{l})$$
- $$\Delta n_g = 6 - \frac{15}{2} = -\frac{3}{2}$$
- $$\Delta H = \Delta U + \Delta n_g RT$$
- $$= -3263.9 + \left(-\frac{3}{2}\right) \times 8.314 \times 10^{-3} \times 298$$
- $$= -3263.9 - (3.71) = -3267.6 \text{ kJ/mol}^{-1}$$
12. (b)
- $$\Delta H = \Delta U + \Delta n_g RT$$
- $$2\text{HI}(\text{g}) \rightarrow \text{H}_2(\text{g}) + \text{I}_2(\text{g}); \Delta n_g = (1+1) - 2 = 0$$
- $$\therefore \Delta H = \Delta U$$
13. (a)
- $$\text{C}_7\text{H}_{16}(\text{l}) + 11\text{O}_2(\text{g}) \xrightarrow{\Delta} 7\text{CO}_2(\text{g}) + 8\text{H}_2\text{O}(\text{l})$$
- $$\Delta H - \Delta U = \Delta n_g RT$$
- $$\therefore \Delta n_g = 7 - 11 = -4 \quad \therefore \Delta H - \Delta U = -4RT$$
14. (a)
- We know that heat and work are not state functions but $q + w = \Delta U$ is a state function. $H - TS = G$ is also a state function.
15. (c)
- $$\Delta U = nC_v \Delta T = 5 \times 28 \times 100 = 14 \text{ kJ}$$
- $$\Delta(PV) = nR(T_2 - T_1) = 5 \times 8 \times 100 = 4 \text{ kJ}$$
16. (a)
- Given: $n = 3$
- $$T_1 = 300; T_2 = 1000$$
- $$C_p = 23 + 0.01T$$

The relation between ΔH and C_p

$$\Delta H = \int_{T_1}^{T_2} nC_p dT \quad \dots\dots(i)$$

After putting all variable values in equation (i), we get

$$\begin{aligned} \Delta H &= n \int_{300}^{1000} (23 + 0.01T) dT = 3 \left[23T + \frac{0.01T^2}{2} \right]_{300}^{1000} \\ &= 3 \left[23(1000 - 300) \right] + 3 \left[\frac{0.01}{2} (1000^2 - 300^2) \right] \\ &= 61950 \text{ J} = 61.95 \text{ kJ} \approx 62 \text{ kJ} \end{aligned}$$

17. (d)
In expansion against vacuum,
 $P_{\text{ext}} = 0 \Rightarrow w = -P_{\text{ext}} \Delta V = 0$
18. (c)
 $\Delta_{\text{sol}}.H^\circ = \Delta_{\text{lattice}}.H^\circ + \Delta_{\text{Hyd}}.H^\circ$
 $4 = 788 + \Delta_{\text{Hyd}}.H^\circ$
 $\Delta_{\text{Hyd}}.H^\circ = -784 \text{ kJ mol}^{-1}$
19. (c)
 $\Delta H_{\text{atomisation}} = \Delta H_{\text{vap}} + \text{Bond energy}$
Hence, $x > y$.
20. (a)
A system at higher temperature has greater entropy (randomness). S and ΔS are related with T as:
 $S_T = \int_0^T \frac{nC_p dT}{T}$ and $\Delta S = \int \frac{dq}{T}$
Thus, both S and ΔS are function of temperature.
21. (a)
 $H = U + PV$ (By definition)
 $\Delta H = \Delta U + \Delta(PV)$ at constant pressure
 $\Delta H = \Delta U + P\Delta V$
22. (b)
For a spontaneous process Gibbs free energy value is negative at constant temperature and pressure i.e., $\Delta G_{T,P} < 0$.
(B) In isobaric pressure, pressure remains constant i.e., $\Delta P = 0$ while in isothermal process, temperature remains constant i.e., $\Delta T = 0$.
(C) $\Delta H_{\text{reaction}} = (\sum \text{bond energies of reactants}) - (\sum \text{bond energies of products})$
(D) In exothermic process, energy is released. So, the value of enthalpy is negative i.e., $\Delta H < 0$.

23. (a)
 $\Delta G = \Delta H - T\Delta S \quad \because \Delta S_g > \Delta S_l > \Delta S_s$
 $\therefore$ On melting the entropy increases and ΔG becomes more negative and hence it becomes easier to reduce metal.
24. (c)
 $\Delta_f H = \sum \Delta_c H(\text{Reactant}) - \sum \Delta_c H(\text{Product})$
 $= 3 \times (-1300) - (-3268) = -632 \text{ kJ mol}^{-1}$
25. (c)

$$\text{C}_2\text{H}_6(\text{g}) + \frac{7}{2}\text{O}_2(\text{g}) \longrightarrow 2\text{CO}_2(\text{g}) + 3\text{H}_2\text{O}(\text{l})$$
Heat of combustion
 $= \sum \Delta_f H_{(\text{products})} - \sum \Delta_f H_{(\text{reactants})}$
 $\Delta_c H(\text{C}_2\text{H}_6, \text{g}) = 2\Delta_c H(\text{C, graphite}) + 3\Delta_c H(\text{H}_2, \text{g}) - \Delta_f H(\text{O}_2, \text{g}) - \Delta_f H(\text{C}_2\text{H}_6, \text{g})$
 $= -1560 = 2(-394) + 3(-286) - 0 - \Delta_f H(\text{C}_2\text{H}_6, \text{g})$
 $\Rightarrow \Delta_f H(\text{C}_2\text{H}_6, \text{g}) = -86 \text{ kJ mol}^{-1}$
26. (d)
Since in adiabatic system, no heat exchange between system and surrounding, hence when methane undergoes combustion, due to endothermic reaction, the temperature rises in container (A)
 $\text{CH}_4 + 2\text{O}_2 \rightarrow \text{CO}_2 + 2\text{H}_2\text{O} + \text{Heat}$
In diathermic container, heat can change between system and surrounding, hence heat release into the surrounding, hence heat releases into the surrounding and temperature of system (B) remains same.
27. (c)
The most appropriate relations are given in B and C only.
28. (b)
Given equation
(A) $2\text{CO}(\text{g}) + \text{O}_2(\text{g}) \longrightarrow 2\text{CO}_2(\text{g}), \Delta H_1^\circ = -x \text{ kJ mol}^{-1}$
(B) $\text{C}(\text{graphite}) + \text{O}_2(\text{g}) \longrightarrow \text{CO}_2(\text{g}), \Delta H_2^\circ = -y \text{ kJ mol}^{-1}$
We have to find ΔH° for the reaction,
 $\text{C}(\text{graphite}) + \frac{1}{2}\text{O}_2(\text{g}) \longrightarrow \text{CO}(\text{g}) \quad \dots(\text{i})$
 $\text{CO}_2(\text{g}) \longrightarrow \text{CO}(\text{g}) + \frac{1}{2}\text{O}_2(\text{g}) \quad \dots(\text{ii})$
 $\Delta H_1 = \frac{x}{2} \text{ kJ/mole}$
 $\text{C}(\text{graphite}) + \text{O}_2(\text{g}) \longrightarrow \text{CO}_2(\text{g}) \quad \dots(\text{iii})$
 $\Delta H_2 = -y \text{ kJ/mol}^{-1}$
Eq. (i) = Eq. (ii) + Eq. (iii)

$$\Delta H = \frac{x}{2} - y$$

$$\Rightarrow \Delta H = \frac{x - 2y}{2}$$

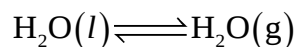
29. (a)
 For free expansion, $p_{\text{external}} = 0$
 $\therefore$ Work done, $W = -p_{\text{ext}}\Delta V = 0$
 $\therefore$ Adiabatic process, $q = 0$
 Also from 1st laws of thermodynamics.
 $\Delta U = q + W$
 $\Delta U = 0$
 Internal energy is a function of temperature.
 If internal energy is constant
 $\Delta T = 0$
 So, for free expansion, $q = 0$, $\Delta T = 0$, $W = 0$
 Hence, option (a) is correct.

30. (b)
 Both A and R are true and R is the correct explanation of A. The enthalpy of neutralization of strong acid and strong base is always -57 kJ/mol . The reason for that is, strong monoacid gives one mole of H^+ and strong mono base gives on mole of OH^- which form one mole of water.
31. (a)
 Among the given options (a) is incorrect. Its correct form is :
 $(\Delta G)_{\text{K}}$ is positive for non-spontaneous reaction.

SECTION-II

1. (557)
 $\Delta H = \Delta U + \Delta(PV) = \Delta U + V\Delta P \quad (\because \Delta V = 0)$
 Or $\Delta U = \Delta H - V\Delta P = -560 - [1(40 - 70) \times 0.1]$
 $= -560 + 3 = -557 \text{ kJ mol}^{-1}$
 So, the magnitude is 557 kJ mol^{-1}
2. (-13538)
 From $\Delta H^\circ = \Delta U^\circ + \Delta n_g RT$
 $\Delta H^\circ = -20 \times 1000 - 1 \times 8.314 \text{ J/mol.K} \times 298 \text{ K}$
 $= -22477.57 \text{ J}$
 $\Delta G^\circ = \Delta H^\circ - T\Delta S^\circ = -22477.57 - (298 \times (-30))$
 $= -13538 \text{ J}$
3. (189494)
 $\Delta H = \Delta U + \Delta n_g RT$

$$n = \frac{90}{18} = 5 \text{ mol}$$

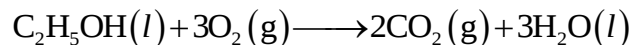


$$\Delta n = 1$$

$$41000 = \Delta U + 1 \times 8.314 \times 373 \Rightarrow \Delta U = 37898.875 \text{ J}$$

$$\text{For 5 moles, } \Delta U = 37898.87 \times 5 = 189494 \text{ J}$$

4. (-326400)



$$\Delta H_c = -327 \text{ kcal}$$

$$\Delta H = \Delta U + \Delta n_g RT$$

$$\Rightarrow -327 \times 10^3 = \Delta U + (-1) \times 2 \times 300$$

$$\Rightarrow \Delta U = -327 \times 10^3 + 600$$

$$\therefore \Delta U = -326400 \text{ cal}$$

5. (5)

$$\Delta G = \Delta H - T\Delta S$$

$$\Delta G = -57.8 - 298 \times (-176 \times 10^{-3}) = -5 \text{ kJ mol}^{-1}$$

6. (50)

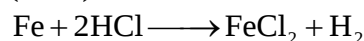
$$q = 150 \text{ joules}$$

$$w = -200 \text{ Joules}$$

$$\Delta E = q + w \quad (\text{First law of thermodynamics})$$

$$\Rightarrow \Delta E = 150 + (-200) = -50 \text{ Joules}$$

7. (2218)



$$\text{No. of moles Fe} = \frac{50}{55.85} \text{ moles}$$

$$\text{No. of moles of H}_2 \text{ produced} = \frac{50}{55.85} \text{ moles}$$

$$\text{Work done} = -P_{\text{ext}}; \Delta V = -\Delta n_g RT$$

$$= \frac{50}{55.85} \times 8.314 \times 298 \approx 2218 \text{ J}$$

8. (718)

$$\Delta_f H^\circ_{\text{KCl}} = \Delta_{\text{sub}} H^\circ_{(\text{K})} + \Delta_{\text{ionization}} H^\circ_{(\text{K})} + \frac{1}{2} \Delta_{\text{bond}} H^\circ_{(\text{Cl}_2)} + \Delta_{\text{electron gain}} H^\circ_{(\text{Cl})} + \Delta_{\text{lattice}} H^\circ_{(\text{KCl})}$$

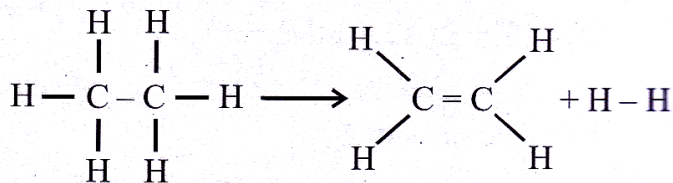
$$\Rightarrow -436.7 = 89.2 + 419 + \frac{1}{2} (243.0) + \{-348.6\} + \Delta_{\text{lattice}} H^\circ_{(\text{KCl})}$$

$$\Rightarrow \Delta_{\text{lattice}} H^\circ_{(\text{KCl})} = -717.8 \text{ kJ mol}^{-1} \approx 718 \text{ kJ mol}^{-1}$$

9. (101)

$$\Delta H_{\text{sub}} = \Delta H_{\text{fus.}} + \Delta H_{\text{vap.}} = 2.8 + 98.2 = 101 \text{ kJ/mol}$$

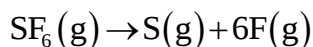
10. (128)



$$\Delta_f H = \sum \text{B.E.}_{\text{Reactant}} - \sum \text{B.E.}_{\text{Products}}$$

$$\begin{aligned} \Delta_f H &= \left[(\text{B.E.})_{\text{C-C}} + 6 \times (\text{B.E.})_{\text{C-H}} \right] - \left[(\text{B.E.})_{\text{C=C}} + 4 \times (\text{B.E.})_{\text{C-H}} + (\text{B.E.})_{\text{H-H}} \right] \\ &= [347 + 6 \times 414] - [611 + 4 \times 414 + 436] = 128 \text{ kJ mol}^{-1} \end{aligned}$$

11. (309)



$$\begin{aligned} \Delta H^\circ &= \Delta H_f^\circ(\text{S}) + 6\Delta H_f^\circ(\text{F}) - \Delta H_f^\circ(\text{SF}_6) \\ &= 275 + 6 \times 80 - (-1100) = 1855 \text{ kJ mol}^{-1} \end{aligned}$$

$$\text{Also, } \Delta H^\circ = 6\Delta H_{\text{S-F}}$$

$$\therefore \Delta H_{\text{S-F}} = \frac{1855}{6} = 309.17 \approx 309 \text{ kJ mol}^{-1}$$

12. (3)

State Variable is an independent variable of a state function.

13. (2)

$$C_{m,p} - C_{m,v} = R \Rightarrow 20.785 - C_{m,v} = 8.314$$

$$\Rightarrow C_{m,v} = 12.471 \text{ J K}^{-1} \text{ mol}^{-1}$$

$$\Delta U = nC_{m,v}\Delta T$$

$$\Rightarrow n = \frac{5000}{12.471 \times (500 - 300)} \Rightarrow n = 2$$

14. (200)

$$\text{Moles of coal} = \frac{2.4}{12} = 0.2$$

$$q = C_v dT$$

$$q = 20 \times (300 - 298) = 40 \text{ kJ}$$

$$0.2 \text{ moles evolved} = 40 \text{ kJ}$$

$$1 \text{ moles evolved} = \frac{40}{0.2} = 200 \text{ kJ/mol}$$

$$\Delta H = -200 \text{ kJ/mol}$$

15. (1718)

$$w = -2.303nRT \log \frac{V_2}{V_1}$$

$$P_1 V_1 = P_2 V_2 \Rightarrow \frac{V_2}{V_1} = \frac{P_1}{P_2} = \frac{6}{3} = 2$$

$$w = -2.303 \times 1 \times 300 \times \log(2)$$

$$\Rightarrow w = -1718.1 \text{ J}$$

16. (117)

Molar mass of $\text{NH}_3 = 17 \text{ g/mol}$

$$\text{Moles of } \text{NH}_3 \text{ given} = \frac{17}{17} = 1 \text{ mole}$$

For 1 mole enthalpy change = 23.4 kJ

5 moles enthalpy change = $23.4 \times 5 = 117 \text{ kJ}$

17. (0)

For free expansion : $w = -P_{\text{ext}} dV$

$$P_{\text{ext}} = 0; w = 0$$

Isothermal expansion, $\Delta U = 0$

$$\Delta U = q + w = q = -w = 0$$

18. (8630)

$$n = 5 \text{ mol}; T = 300 \text{ K}; V_1 = 10 \text{ L}; V_2 = 20 \text{ L}$$

Work done in isothermal condition.

$$w_{\text{rev}} = -nRT \ln \frac{V_2}{V_1}$$

$$= -5 \times 8.3 \times 300 \ln \frac{20}{10} = -8630.38 \text{ J}$$

19. (300)

$$\Delta G = \Delta H - T\Delta S = 0 \text{ at equilibrium}$$

$$\Rightarrow -165 \times 10^3 - T \times (-550) = 0 \Rightarrow T = 300 \text{ K}$$

20. (103.7)



$$\Delta H_1 = -2220 \text{ kJ/mol}$$



$$\Delta H_2 = -393.5 \text{ kJ/mol}$$



$$\Delta H_3 = -285.8 \text{ kJ/mol}$$

Formation of C_3H_8 (1mole) :



Equation (4) obtained by

$$\begin{aligned} & 3 \times \text{Eq}(2) + 4 \times \text{Eq}(3) - \text{Eq}(1) \\ &= 3 \times (-393.5) + 4 \times (-285.8) - (-2220.0) \\ &= -1180.5 - 1143.2 + 2220.0 = -103.7 \text{ kJ/mol} \end{aligned}$$

21. (2)

$$\Delta H_{\text{neutralization}} = -57.3 \text{ kJ/mol}$$

In case of acetic acid

$$\Delta H = \Delta H_{\text{ioni}} + \Delta H_{\text{neutralization}}$$

$$-55.3 = \Delta H_{\text{ioni}} - 57.3$$

$$\Delta H_{\text{ioni}} = 2 \text{ kJ/mol}$$

22. (727)

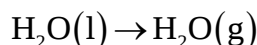
$$\Delta U = -726 \text{ kJ/mol}$$

$$\Delta n_g = 1 - 3/2 = -1/2$$

$$\Delta H = \Delta U + \Delta n_g RT$$

$$= -726 - \frac{1}{2} \times \frac{8.3 \times 300}{1000} = -727.245$$

23. (38)



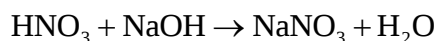
$$\Delta n_g = \sum n_p - \sum n_R = 1 - 0 = 1$$

$$\Delta H = \Delta U + \Delta n_g RT$$

$$\Delta U = \Delta H - \Delta n_g RT$$

$$= 41.1 - \frac{1 \times 8.31 \times 373}{1000} \text{ kJ/mol} = 38 \text{ kJ/mol}$$

24. (54)



Start 120 40

End 80 0 40 mmol

$$\Delta_f H = 40 \text{ mmol} \times (57 \times 10^3) \text{ J mol}^{-1}$$

$$= 40 \times 10^{-3} \text{ mol} \times 57 \times 10^3 \text{ J mol}^{-1} = 2280 \text{ J}$$

$$m \Delta T = 2280 \Rightarrow 1000 \text{ g} \times 4.2 \times \Delta T = 2280$$

$$\Delta T = \frac{2280}{4.2} \times 10^{-3} = \frac{22800}{42} \times 10^{-3} = 542.86 \times 10^{-3}$$

$$= 54.286 \times 10^{-2} \text{ K} = 54.286 \times 10^{-2} \text{ }^{\circ}\text{C}$$

25. (4)

Extensive properties Mole, volume, Gibbs free energy

Intensive properties Mole mass, molar heat capacity, molarity, E_{cell}°

Thus, total number of intensive properties are 4.

26. (1200)

Power of heater = 60 W

$$= 60 \text{ J/s}$$

Total energy emitted = 60×100

$$= 6000 \text{ J}$$

Heat capacity $\times$ temperature difference = total energy emitted

Heat capacity $\times 5^{\circ}\text{C} = 6000$

$$\text{Heat capacity} = \frac{6000}{5} = 1200 \text{ J/K}$$

27. (150)

Given, Number of moles = 1 mole

Temperature (T_i) = $27^{\circ}\text{C} = 300 \text{ K}$

Since, the processes is adiabatic, hence,

$$q = 0$$

$$\Rightarrow W = \Delta U$$

On substituting values, we will get

$$W = nC_V \Delta T$$

$$-3 \times 10^3 = 1 \times 20 [T_2 - 300]$$

$$T_2 - 300 = -150 \text{ or } T_2 = 150 \text{ K}$$

28. (0)

For in isothermal processes, the temperature remains constant.

So, the change in internal energy is zero.

29. (620)

$1 \rightarrow 2 \Rightarrow$ Isobaric processes

$2 \rightarrow 3 \Rightarrow$ Isochoric processes

$3 \rightarrow 1 \Rightarrow$ Isothermal processes

Work done

$$(W) = W_{1 \rightarrow 2} + W_{2 \rightarrow 3} + W_{3 \rightarrow 1}$$

$$= \left(-p(V_2 - V_1) + 0 + \left[-p_1 V_1 \ln \left(\frac{V_2}{V_1} \right) \right] \right)$$

$$= \left[-1 \times (40 - 20) + 0 + 0 \left[-1 \times 20 \ln \left(\frac{20}{40} \right) \right] \right]$$

$$= -6.2 \text{ bar L}$$

$$|W| = 6.2 \text{ bar L} = 620 \text{ L}$$

30. (3)

Given $n = 1$, $R = 8.314 \text{ JK}^{-1}\text{mol}^{-1}$

$$V_2 = 3L, V_1 = 2L$$

$$\begin{aligned}\Rightarrow \Delta S_{\text{system}} &= nR \ln \left(\frac{V_2}{V_1} \right) \\ &= 1 \times 8.314 \ln \left(\frac{3}{2} \right) \\ &= 3.37 \text{ JK}^{-1}\end{aligned}$$

$$\Delta S_{\text{surroundings}} = 3.37 \approx 3 \text{ JK}^{-1}$$

31. (10)

Reaction, $A \rightleftharpoons B$ at 298 K

Given, $\Delta H^\circ = -54.07 \text{ kJ/mol}$

$$\Delta S^\circ = 10 \text{ J/K/mol}$$

We know that,

$$\Delta G^\circ = \Delta H^\circ - T\Delta S^\circ$$

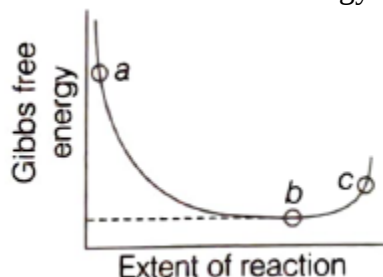
$$\text{or } -2.303RT \log K = -54070 - 298 \times 10$$

$$-5705 \times \log K = -57050$$

$$\text{So, } \log K = 10$$

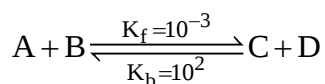
32. (2)

Graph between Gibbs free energy vs extent of reaction.



- At a point we observe $\Delta_r G < 0$
So, reaction is spontaneous.
- At b point $\Delta G = 0$ (equilibrium)
- At c point Gibbs free energy $\Delta_r G > 0$
So, reaction is non-spontaneous
- Two statements B and C are correct (2).

33. (6)



Sine, equilibrium constant can be calculated as

$$K_{\text{eq}} = \frac{K_f}{K_b} \text{ or, } k_{\text{eq}} = \frac{10^3}{10^2} = 10$$

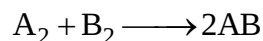
Again, the relation between ΔG° and K_{eq} can be calculated from the formula

$$\Delta G^\circ = -RT \ln K$$

So, $\Delta G^\circ = -8.3 \times 300 \times \ln(10)$

or $\Delta G^\circ = -5.7 \text{ kJ/mol} \approx -6 \text{ kJ/mol}$

34. (800)



$$\Delta H_f^\circ(AB) = -200 \text{ kJ mol}^{-1}$$

$\therefore \Delta H_f^\circ$ for reaction

$$A_2 + B_2 \longrightarrow 2AB \text{ is } -400 \text{ kJ mol}^{-1}$$

Given that, bond enthalpy of A_2 , B_2 and AB is 1 : 0.5 : 1.

Assume that bond enthalpy of A_2 is $x \text{ kJ mol}^{-1}$

$$\therefore \text{Bond enthalpy of } B_2 = 0.5x \text{ kJ mol}^{-1}$$

$$\begin{aligned} \therefore \text{Bond enthalpy } AB &= x \text{ kJ/mol} \\ &= (BE)_{A_2} + (BE)_{B_2} - 2(BE)_{AB} \end{aligned}$$

$$\Rightarrow \Delta H_r^\circ = -400 \text{ kJ mol}^{-1}$$

$$\begin{aligned} \Rightarrow -400 &= x + 0.5x - 2x \\ x &= 800 \text{ kJ mol}^{-1} \end{aligned}$$

35. (4)

A $\rightarrow$ Endothermic (atomisation)

B $\rightarrow$ Endothermic (atomisation)

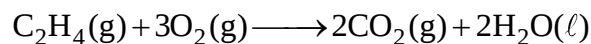
C $\rightarrow$ Endothermic (vaporisation)

D $\rightarrow$ Exothermic (combustion)

E $\rightarrow$ Endothermic (dissolution)

36. (1411)

Consider the following reaction



$$\Delta U = -1406 \text{ kJ mol}^{-1}$$

$$\Delta H = \Delta U + \Delta n_g RT$$

$$= -1406 + \frac{(-2) \times 8.314 \times 300}{1000}$$

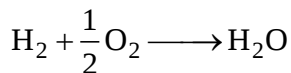
$$= -1406 - 4.98$$

$$\approx -1411 \text{ kJ mol}^{-1}$$

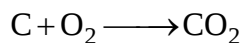
The minimum value of $T\Delta S$ at equilibrium, $T\Delta S = -1411 \text{ kJ}$

[$\because \Delta G = \Delta H - T\Delta S \Rightarrow$ at equilibrium $\Delta G = 0 \Rightarrow T\Delta S = \Delta H$]

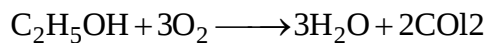
37. (278)



$$\Delta H = -241.8 \text{ kJ/mol} \quad \dots(\text{i})$$

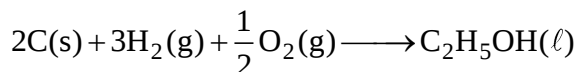


$$\Delta H = -393.5 \text{ kJ/mol} \quad \dots(\text{ii})$$



$$\Delta H = -1234.7 \text{ kJ/mol} \quad \dots(\text{iii})$$

Formation of $\text{C}_2\text{H}_5\text{OH}$ will be



Heat of formation of $\text{C}_2\text{H}_5\text{OH}(\ell) = \text{Eq. (ii)} + 3 \times \text{Eq. (i)} - \text{Eq. (iii)}$

$$2 \times (-393.5) + 3 \times (-241.8) - (0 - 1234.7)$$

$$= -787 - 725.4 + 1234.7$$

$$= -277.7$$

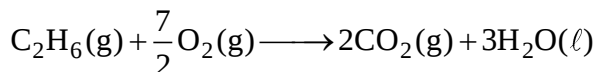
$$\approx -278 \text{ kJ/mol}$$

38. (1006)

Heat released by combustion of 1 mole of

$$\text{C}_2\text{H}_6 = \Delta U = \frac{-20 \times 0.5}{0.3} \times 30$$

$$= -1000 \text{ kJ}$$



$$\Delta n = 2 - \left(1 + \frac{7}{2}\right) = -\frac{5}{2}$$

$$\Delta H = \Delta U + \Delta n_g RT$$

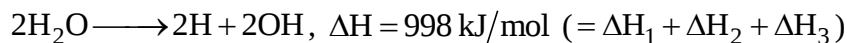
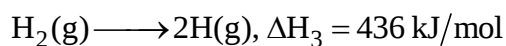
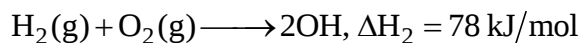
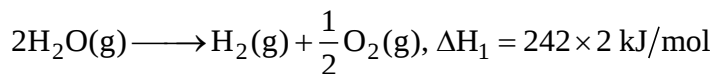
$$= -1000 - \frac{5}{2} \times 8.3 \times 10^{-3} \times 300 \text{ K}$$

$$= -1000 - 6.225$$

$$= -1006 \text{ kJ}$$

Thus, heat released = 1006 kJ/mol

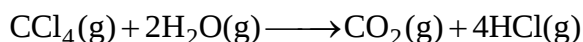
39. (499)



$\Rightarrow$ For 1 mole H_2O ,

$$\Delta H = \frac{998}{2} = 499 \text{ kJ/mol}$$

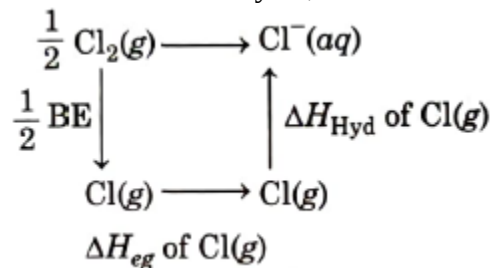
40. (173)



$$\begin{aligned}\Delta H_r &= (\Delta H_f \text{CO}_2 + 4\Delta H_f \text{HCl}) - (\Delta H_f \text{CCl}_4 + 2\Delta H_f \text{H}_2\text{O}) \\ &= [-394 + 4 \times (-92)] - [-105 + 2 \times (-242)] \\ &= -173 \text{ kJ/mol}\end{aligned}$$

41. (610)

From Born Haber cycle,

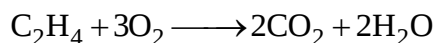


From Hess's heat summation law

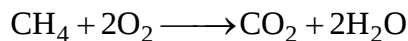
$$\begin{aligned}\Delta H^\circ &= \frac{1}{2} \times \text{BE} + \Delta H_{\text{eg}} + \Delta H_{\text{Hvd}} \\ &= \frac{1}{2} \times 240 + (-350) + (-380) \\ &= 120 - 350 - 380 = -610 \text{ kJ mol}^{-1}\end{aligned}$$

42. (925)

Let volume of C_2H_4 is x litre,



Initial	x	—	—
Final	—	2x	2x



Initial	(16.8 - x)	—
Final	—	(16.8 - x)

$$\text{Total volume of CO}_2 = 2x + 16.8 - x$$

$$\Rightarrow 28 = 16.8 + x \text{ or } x = 11.2 \text{ L}$$

$$\text{Volume of C}_2\text{H}_4 = 11.2 \text{ L}$$

$$\text{Volume of CH}_4 = (16.8 - 11.2) \text{ L} = 5.6 \text{ L}$$

$$\text{No. of moles of CH}_4 = \frac{5.6}{22.47} = 0.25 \text{ mol}$$

$$\text{No. of moles of C}_2\text{H}_4 = \frac{11.2}{22.4} = 0.5 \text{ mol}$$

So, the heat evolved will be

$$\Rightarrow 0.25(-900) + 0.5(-1400) = -925 \text{ kJ}$$

43. (360)

Energy utilised by the athlete

= 50% of 1800 kJ

$$= \frac{50}{100} \times 1800 = 900 \text{ kJ}$$

Utilised energy of athlete = $n_{\text{H}_2\text{O}} \times 45$

$$900 = n_{\text{H}_2\text{O}} \times 45$$

$$\Rightarrow n_{\text{H}_2\text{O}} = 20 \text{ mol}$$

$$W_{\text{H}_2\text{O}} = 20 \times 18 = 360 \text{ g}$$

44. (38)

Given,

$$\Delta H_{\text{vapour}}^{\circ} = +40.79 \text{ kJ/mol}$$

$$T = 100^{\circ}\text{C} = 373 \text{ K}$$

Using enthalpy equation,

$$\Delta H_{\text{vapour}}^{\circ} = \Delta U^{\circ} + \Delta n_g RT$$

$$\Delta U^{\circ} = 40.79 - \frac{8.3 \times 373}{1000}$$

$$= 37.67 \text{ kJ/mol} \approx 38 \text{ kJ/mol}$$

45. (55)

Given, $V_1 = 100 \text{ L}$ and $V_2 = 10 \text{ L}$

Work done is given,

$$W = -nRT \ln \frac{V_2}{V_1}$$

$$= -1 \times 0.08206 \times 291.15 \times 2.303 \log \frac{10}{100}$$

$$= 55 \text{ L atm}$$

Hence, final answer is 55 L atm.

46. (274)

In adiabatic condition, $q = 0$

Then, equation for change in internal energy will be given by

$$\Delta U = q + W \quad (q = 0)$$

$$nC_V \Delta T = -p_{\text{ext}} (V_2 - V_1) \quad \dots(i)$$

as $(W = p \Delta V)$

$$V_2 = 2V_1 \quad (\text{given})$$

$$\frac{nRT_2}{P_2} = \frac{2nRT_1}{P_1} \quad \dots(ii)$$

$$p_1 = 5 \text{ atm}, T_1 = 298 \text{ K}$$

p_2 from Eq. (ii) will be

$$p_2 = \frac{5T_2}{2 \times 298}$$

Now from Eq. (i)

(Put $p_{\text{ext}} = 1 \text{ atm}$)

$$n \frac{5}{2} R (T_2 - T_1) = -1 \left[\frac{nRT_2}{p_2} - \frac{2nRT_1}{p_1} \right]$$

Put, $T_1 = 298$ and $p_2 = \frac{5T_2}{2 \times 298}$

$$\frac{5n}{2} R [T_2 - 298] = nR \left[\frac{T_1}{5} - \frac{T_2}{\left(\frac{5T_2}{2 \times 298} \right)} \right] \quad \dots(\text{iii})$$

On solving Eq. (iii)

$$T_2 = 274.16 \text{ K}$$

Hence, nearest integer value of temperature is 274 K.

47. (200)

For isothermal process, $\Delta U = 0$

So, $Q = -W$

$$= -[-p_{\text{ext}} (V_2 - V_1)]$$

$$Q = 5[20 - 60]$$

$$= -200 \text{ atm L}$$

48. (28721)

It is isothermal reversible expansion, so work done is negative.

Work done is given by

$$W = -2.303nRT \log \left(\frac{V_2}{V_1} \right)$$

$$= -2.303 \times 5 \times 8.314 \times 300 \log \left(\frac{100}{10} \right)$$

$$= -28720.713 \text{ J}$$

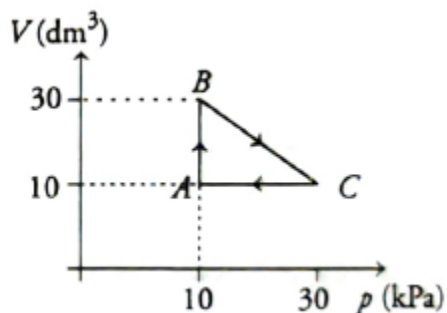
$$\approx -28721 \text{ J}$$

Hence, the value of x is 28721.

49. (200)

Work done is given by area enclosed in the p vs V cyclic graph.

Sign is +ve for clockwise cyclic process for V vs p graph.



Work done = Area of triangle

$$\begin{aligned}
 &= \frac{1}{2} \times \text{base} \times \text{height} \\
 &= \frac{1}{2} \times 20 \times 20 \\
 &= 200 \text{ J}
 \end{aligned}$$

Hence, work done is 200 J.

50. (1200)

For isothermal expansion at constant pressure, heat is given by

$$\begin{aligned}
 Q &= -p_{\text{ext}} (V_2 - V_1) \\
 &= -80 \times 1000 \times (45 - 30) \times 10^{-3} \\
 &= -15 \times 80 = -1200 \text{ J}
 \end{aligned}$$

Negative sign indicates heat is lost.

Hence, amount of heat transfer is 1200 J.

51. (400)

Given,

$$\Delta H_{\text{vap}} = 30 \text{ kJ/mol}$$

$$\Delta S_{\text{vap}} = 75 \text{ J mol}^{-1} \text{K}^{-1}$$

$$T = ?$$

At equilibrium, $\Delta G = 0$

$$\Delta H_{\text{vap}} = T \Delta S_{\text{vap}}$$

$$\text{So, } 30 \times 1000 = T \times 75$$

$$T = 400 \text{ K}$$

52. (2000)

From Gibb's free energy equation,

$$\Delta G = \Delta H - T \Delta S$$

For reaction to be spontaneous

$$\Delta G = -ve$$

For limiting case $\Delta G = 0$

$$\Delta H = T \Delta S$$

$$T = \frac{\Delta H}{\Delta S} = \frac{400 \text{ kJ/mol}}{0.2 \text{ kJ/mol-K}} = 2000 \text{ K}$$

Hence, reaction will become spontaneous above 200 K.

53. (57)

$$\Delta G^\circ = -RT \ln K_{\text{eq}}$$

$$= -2.303RT \log K_{\text{eq}}$$

$$= -2.303 \times 8.314 \times 300 \times \log 10$$

$$= -5744.14 \text{ J/mol}$$

$$= -5.744 \text{ kJ/mol}$$

$$= -57.44 \times 10^{-1} \text{ kJ/mol}$$

Thus, the value is 57.

54. (37)
 Given, $T = 400 \text{ K}$
 $\Delta H^\ominus = 77.2 \text{ kJ/mol}$
 $\Delta S = 122 \text{ JK}^{-1}$
 Free energy is given by
 $\Delta G^\ominus = \Delta H^\ominus - T\Delta S^\ominus$
 $= 77.2 \times 10^3 - 400 \times 122$
 $= 28400 \text{ J}$
 $\Delta G^\ominus = -2.303 RT \log K$
 $28400 = -2.303 \times 8.314 \times 400 \times \log K$
 $\log K = -3.708$
 or $\log K = -37.08 \times 10^{-1}$
 Hence, the missing value is 37.

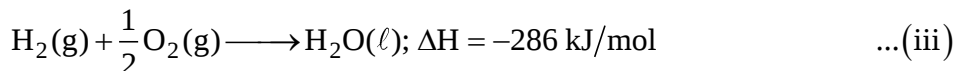
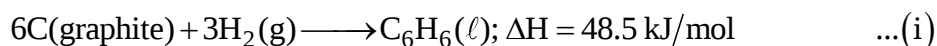
55. (2)
 According to question
 $\text{H}^+ + \text{OH}^- \longrightarrow \text{H}_2\text{O} \Rightarrow x \text{ (for HCl)}$
 $2\text{H}^+ + 2\text{OH}^- \longrightarrow 2\text{H}_2\text{O}$
 $\Rightarrow 2x = y \text{ (for H}_2\text{SO}_4\text{)}$
 $\Rightarrow \frac{y}{x} = 2$

56. (82)
 $\text{CuSO}_4(\text{s}) + \text{H}_2\text{O}(\ell) \longrightarrow \text{CuSO}_4(\text{aq}); \Delta H = -70 \text{ kJ} \quad \dots(\text{i})$
 $\text{CuSO}_4 \cdot 5\text{H}_2\text{O}(\text{s}) + \text{H}_2\text{O}(\ell) \longrightarrow \text{CuSO}_4(\text{aq}); \Delta H = 12 \text{ kJ} \quad \dots(\text{ii})$
 Subtracting Eqs. (i) and (ii)
 $\text{CuSO}_4 + 5\text{H}_2\text{O} \longrightarrow \text{CuSO}_4 \cdot 5\text{H}_2\text{O}; \Delta H = -70 - 12 = -82 \text{ kJ}$

57. (150)
 The complete reaction is as follow,
 $\text{C}_6\text{H}_5\text{COOH}(\text{s}) + \frac{15}{2} \text{O}_2(\text{g}) \longrightarrow 7\text{CO}_2(\text{g}) + 3\text{H}_2\text{O}(\ell)$
 $\Delta H = \Delta U + \Delta n_g RT$
 $= -321.30 - \frac{1}{2} \frac{R}{100} \times 300$
 $= (-321.30 - 150R) \text{ kJ}$
 Matching with equation given in question the value of x is 150.

58. (6535)

Given,



$$\begin{aligned} \text{Eq. (i)} \times 1 + (\text{ii}) \times 6 + (\text{iii}) \times 3 \\ = -48.5 - 6 \times 393.5 - 3 \times 286 \\ = -3267.5 \text{ kJ 1 mol} \\ = -6535 \text{ kJ for 2 mol} \end{aligned}$$

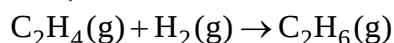
59. (125)

Given, Bond enthalpies of

C–H = 414 kJ; C–C = 347 kJ

H–H = 435 kJ; C=C = 615 kJ

Now, the formation of ethane takes place as follows



$$\Delta H = \text{B.E.}(\text{C}=\text{C}) + 4\text{B.E.}(\text{C}-\text{H}) + \text{B.E.}(\text{H}-\text{H}) - \text{B.E.}(\text{C}-\text{C}) - 6\text{B.E.}(\text{C}-\text{H})$$

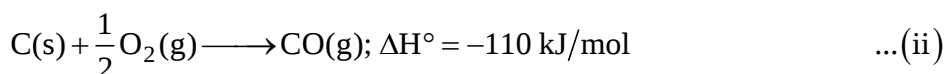
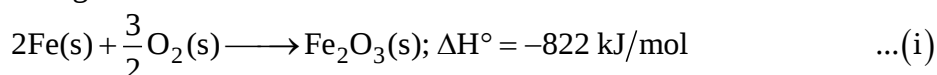
$$\Delta H = \text{B.E.}(\text{C}=\text{C}) + \text{B.E.}(\text{H}-\text{H}) - \text{B.E.}(\text{C}-\text{C}) - 2\text{B.E.}(\text{C}-\text{H})$$

$$\Rightarrow \Delta H = 615 + 435 - 347 - 2(414)$$

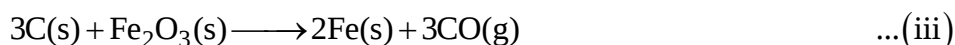
$$\Delta H = -125 \text{ kJ}$$

60. (492)

Two given reactions are



Multiply Eq. (ii) by 3 and then subtract Eq. (i) from this equation to get the required equation.



$$\begin{aligned} \text{Then, } \Delta H_3 &= 3 \times \Delta H_2 - \Delta H_1 \\ &= 3(-110) - (-822) \\ &= 492 \text{ kJ/mol} \end{aligned}$$

Hence, enthalpy change is 492 kJ/mol

61. (56)

Given,

$$\Delta H_{\text{vapour}}^\circ \text{CCl}_4 = 30.5 \text{ kJ/mol}$$

$$\text{Mass of CCl}_4 = 284 \text{ g}$$

$$\text{Molar mass of CCl}_4 = 154 \text{ g/mol}$$

$$\text{Moles of CCl}_4 = \frac{284}{154} = 1.844 \text{ mol}$$

$\Delta H_{\text{vapour}}^{\circ}$ for 1 mole = 30.5 kJ/mole

$\Delta H_{\text{vapour}}^{\circ}$ for 1.844 mole

$$= 30.5 \times 1.844$$

$$= 56.242 \text{ kJ}$$

Hence, final answer is 56 kJ (nearest integer).

EXERCISE - 2 [A]

1. (a)

$$\Delta S = nC_V \ln \frac{T_f}{T_i} + nR \ln \frac{V_f}{V_i}$$

$$= 2R \ln 2 = 11.5$$

2. (a)

$$\int \frac{C_p}{T} dT = \int \frac{dQ}{T} = \Delta S$$

3. (c)

Entropy change of universe is always positive

4. (a)

$$w = nRT \ln \frac{V_f}{V_i}$$

$$= 2.5 \times 8.314 \times 310 \ln \frac{2.5 \times 8.314 \times 310}{58 \times 10^3}$$

$$= 44665$$

5. (c)

At 0°C ice & water have same G.

6. (d)

- (a) In melting $\Delta V > 0 \Rightarrow W < 0$
- (b) In melting of ice $\Delta V < 0 \Rightarrow W > 0$
- (c) In expansion $\Delta V > 0 \Rightarrow W < 0$
- (d) In expansion against vacuum
 $W = 0, Q = 0, \Delta U = \Delta H = 0$

7. (a)

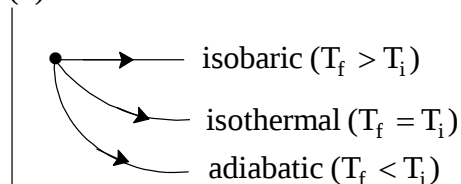
$$\text{For bath } \Delta S = \frac{Q}{T_{\text{Bath}}}$$

$$\text{For glass } \Delta S = \frac{Q}{T_{\text{glass}}}$$

Since $T_{\text{bath}} < T_{\text{glass}}$

$$\text{So, } |\Delta S_{\text{bath}}| > |\Delta S_{\text{glass}}|$$

8. (b)



9. (d)
 (1) $\Delta n_g = 0$
 (2) $\Delta n_g = -1$
 (3) $\Delta n_g = +1$
 So, $3 > 1 > 2$
10. (a)
 Combustion reaction $\Rightarrow \Delta H = -ve$
 $\Delta n_g < 0 \Rightarrow \Delta S = -ve$
11. (c)
 At equilibrium
 $\Delta G = 0$, So $G_A = G_B$
12. (a)
 $\Delta H_R = -74.9$
 $\Delta S_R = 186.3 - 5.6 - 2 \times 130.7$
 $\Delta G_R = \Delta H_R - T\Delta S_R = -50.8$
13. (d)

$$\Delta G = nRT \ln \frac{P_f}{P_i} = 8.314 \times 293 \ln \frac{1}{2}$$

$$= -1.7 \text{ kJ/mole}$$
14. (c)
 Entropy depends on moles.
15. (c)
 O_3 has highest C_v
16. (c)
 $\Delta U_R = -723 - 8.314 \times 0.3 \times (-1) = -69.8 \text{ kJ/mole}$
 $n_{C_2H_4} = 3.5, n_{HCl} = 3$
 So $\Delta U = -69.8 \times 3 \text{ kJ} = -209.4$
17. (a)

$$w = -600R \ln \frac{1}{2} - 2R(400 - 300) - 800R \ln 2 - 2R(300 - 400)$$

$$= -200R \ln 2 = -100R \ln 4$$
18. (c)
 $-3000 = 1 \times 20 \times (T_f - 300)$
 $T_f = 150K$

19. (d)

$$2 \times \frac{5}{2} R \times (T_f - 350) = -2 \left(\frac{2RT_f}{2} - \frac{2R \times 350}{1} \right)$$

$$\Rightarrow \frac{5}{2} T_f - \frac{5}{2} \times 350 = -T_f + 700$$

$$\Rightarrow \frac{7}{2} T_f = \frac{9}{2} \times 350 \Rightarrow T_f = 450 \text{ K}$$

$$w = 2 \times \frac{5}{2} R \times (450 - 350) = 500R$$

20. (b)

$$\eta = 1 - \frac{298}{373} = 22.2$$

21. (b)

$$1 - \frac{300}{500} = \frac{w}{2} \Rightarrow w = 0.8 \text{ k cal}$$

22. (c)

$$1 - \frac{T_2}{1000} = 1 - \frac{360}{T_2}$$

$$\Rightarrow T_2 = 600$$

23. (a)

$$\Delta H = -3 + (-1) \frac{2 \times 300}{1000} = -3.6 \text{ kcal}$$

$$\Delta G = -3.6 + \frac{10 \times 300}{1000} = -0.6 \text{ kcal}$$

24. (c)

$$\Delta S = nC_v \ln \frac{T_f}{T_i} = 2 \times \frac{3}{2} R \ln \frac{573}{473}$$

25. (d)

At phase equation $\Delta G = 0$

26. (c)

$$\text{H}_2\text{O}(\ell, 1 \text{ atm}, 373 \text{ K}) \longrightarrow \text{H}_2\text{O}(g, 1 \text{ atm}, 373 \text{ K})$$

$$\Delta G = 0$$

$$\text{H}_2\text{O}(g, 1 \text{ atm}, 373 \text{ K}) \longrightarrow \text{H}_2\text{O}(g, 2 \text{ atm}, 373 \text{ K})$$

$$\Delta G = \int V dp = nRT \ln \frac{P_f}{P_i}$$

$$= 373 R \ln 2$$

27. (d)
- $$T_f = \frac{T_H + T_C}{2}$$
- $$\Delta S = \int_{T_H}^{T_f} ms \frac{dT}{T} + \int_{T_C}^{T_f} ms \frac{dT}{T}$$
- $$= C_v \ln \frac{T_f}{T_H} + C_v \ln \frac{T_f}{T_C}$$
- $$= C_v \ln \frac{T_f^2}{T_H T_C} = C_v \ln \frac{(T_H + T_C)^2}{4 T_H T_C}$$
28. (c)
- S° of $H_2 > 0$ at 298 K
29. (a)
- $\Delta H > 0, \quad \Delta S > 0$
 (+ve y intercept) (–ve slope)
30. (a)
- In adiabatic reversible process only
 $T^\gamma P^{1-\gamma} = k$
31. (a)
- $$\Delta S = 2090 \ln \frac{273}{200} + \frac{3.34 \times 10^5}{273} + 4180 \ln \frac{373}{273} + \frac{22.6 \times 10^5}{373} + 2090 \ln \frac{400}{373}$$
- $$= 9390 \text{ J/kg}$$
32. (c)
- $RE = 3X_1 - X_2$
33. (b)
- $\Delta_f H_{H_2O(g)} = x_2 + x_1 T_1$
 So, $\Delta H_{\text{reaction}} = 2x_3 + 3x_2 + 3x_1 T_1 - x_4$
34. (a)
- Q is halved and m is also halved.
35. (b)
- $$\frac{d}{dT} \left(\frac{\Delta G}{T} \right) = \frac{a}{T^2} + \frac{b}{T} = \frac{-\Delta H}{T^2}$$
- $$\Rightarrow \Delta H = -a - bT$$
36. (c)
- $$150 \times 50 \times t = \frac{1 \times 150 \times 10^3}{293 \times 0.0821} \times \frac{7}{2} R \times 17 \quad \Rightarrow \quad t = 6.86 \text{ min}$$

37. (a)

$$\Delta E = 2.25 \times 10^6 - \frac{1000}{18} \times 8.314 \times 373$$

$$= 2.08 \times 10^6$$

38. (b)

$$\Delta U = 1.5nR\Delta T = 3R$$

$$\Delta U \approx 25 \text{ J}$$

$$Q = 42 \text{ J}$$

$$\Rightarrow W = -17 \text{ J}$$

$$-17 = -10^5 \times 8.5 \times 10^{-4} \times h$$

$$h = 20 \text{ cm .}$$

39. (c)

$$-2nRT \ln \frac{V}{1} = \frac{1}{2} \left(-nRT \ln \frac{3}{1} \right)$$

$$\Rightarrow V = \sqrt{3} L$$

$$h = \frac{(\sqrt{3}-1) \times 1000}{16\pi}$$

$$h = 14.5 \text{ cm}$$

EXERCISE - 2 [B]

One or More Than One Option Correct

- (c, d)
Volume & Kinetic energy depend on amount of substance.
- (a, d)
Internal Energy is a state function so it does not depend on path.
It does changes during isothermal change.
- (b, c, d)
For reversible adiabatic process.
 $PV^\gamma = k$, $TV^{\gamma-1} = k$, $T^\gamma P^{1-\gamma} = k$
- (a, b)
E is a state function, which depends on T
- (a, b, d)
For isothermal process, T is constant.
 $P_1 V_1 = P_2 V_2$, $\Delta E = 0$, $\Delta H_1 = H_2$
- (a, b, c)
 $P_i = 2 \text{ bar}$, $T_i = 273 \text{ K}$, $P_f = 4 \text{ bar}$

$$\frac{P}{V} = R \Rightarrow \frac{P_i}{V_i} = \frac{P_f}{V_f} \Rightarrow V_f = 2V_i$$

$$\Rightarrow T_f = \frac{P_f V_f}{P_i V_i} T_i \Rightarrow T_f = 4T_i$$

$$\Rightarrow T_f = 4 \times 273 = 1092 \text{ K}$$

$$\Delta E = 1 \times 12.5 \times (1092 - 273) \\ = 10.24 \text{ kJ}$$

$$C_{\text{process}} = C_V + \frac{R}{1 - (-1)} = 12.5 + \frac{8.314}{2} = 16.657$$

$$Q = 1 \times 16.657 \times (1092 - 273) = 13.64 \text{ kJ}$$

$$W = \Delta E - Q \\ = -3.4 \text{ kJ}$$

7. (a, b, d)

$$2 \times \frac{3}{2} R \times (T_f - T_i) = -1 \times (10 - 1)$$

$$T_f - T_i = \frac{-9}{3R} \Rightarrow T_f = T_i - \frac{3}{R}$$

$$\Rightarrow T_f = 400 - \frac{3}{0.0821} = 363 \text{ K}$$

$$T_{f, \text{rev, adiabatic}} < T_{f, \text{irr, adiabatic}}$$

$$\Delta S_{\text{sys}} = 0 \text{ for adiabatic process.}$$

8. (b, c, d)

For ideal gas

$$dE = dQ + dW = dQ - PdV$$

$$dH = dE + PdV + VdP = dQ + VdP$$

$$dS_m = C_V \frac{dT}{T} + R \frac{dV}{V}$$

$$dG = VdP - SdT$$

9. (c, d)

Heat & work done path functions.

10. (a, b, c)

For adiabatic process $Q = 0$

$$W = \Delta U = nC_V \Delta T = \frac{nR(T_2 - T_1)}{\gamma - 1}$$

$$W = -P_{\text{ext}}(V_f - V_i)$$

$$= -P_{\text{ext}} \left(\frac{nRT_f}{P_f} - \frac{nRT_i}{P_i} \right)$$

11. (a, b, c)

$$\Delta H = \Delta U + \Delta(PV) = \Delta U + P\Delta V + V\Delta P + \Delta P\Delta V$$

12. (a, b, c)
 At 400K & 1 atm $X(\ell)$ is in equilibrium with $X(g)$
 i.e. $\Delta G = 0$
 at constant T

$$\Delta G = nRT \ln \frac{P_2}{P_1}$$
 If $P_2 > P_1$ then $\Delta G = +ve$
 If $P_2 < P_1$, then $\Delta G = -ve$

$$\Delta G = nRT \ln \frac{2}{1} > 0$$

$$\Delta G = nRT \ln \frac{0.1}{1} < 0$$
 Correct option a,b,c

13. (a, c, d)

$$\Delta S = nC_p \ln \frac{T_2}{T_1}$$
 at constant P
 $T_2 > T_1$
 $\Delta S = +ve$

$$\Delta H_2 = \Delta H_1 + \Delta C_p (T_2 - T_1)$$
 $T_2 > T_1$
 $\Delta H_2 > \Delta H_1$
 $\Delta G = \Delta H - T\Delta S$
 $T\Delta S > \Delta H$
 $\Delta G < 0$
 i.e. process is spontaneous correct option a,c,d

14. (a, b, c, d)
 For adiabatic irreversible
 $\Delta S_{sys} \neq 0$
 For isentropic process
 $\Delta S_{sys} = 0$
 $\Delta G_{sys} = \Delta H - T\Delta S < 0$
 If ΔH is positive & ΔS is positive at high T.
 $dG = VdP - SdT$ is applicable for PV only

$$\Delta S_{system} = -\frac{n\Delta H_{vap}}{T} = -\frac{0.5 \times 40600}{373} = -54.42 \text{ JK}^{-1}$$

Comprehension Type

Passage - I

1. (b)

$$W = -nRT \ln \frac{P_i}{P_f}$$

$$W = -P_i V_i \ln \frac{P_i}{P_f}$$

$$W = -2 \times 8 \ln \frac{2}{20} = 36.848 \text{ bar L}$$

2. (c)

$$W = -20 \left(\frac{16}{20} - 8 \right) = -16 + 160 = 144 \text{ L bar}$$

3. (b)

$$\begin{aligned} W &= -10 \left(\frac{16}{10} - 8 \right) - 20 \left(\frac{16}{20} - \frac{16}{10} \right) \\ &= -16 + 80 - 16 + 32 \\ &= 80 \text{ L Bar} \end{aligned}$$

Passage - II

4. (a)

$$\begin{aligned} \Delta H_{\text{neutralisation}} &= q - 55.84 \\ -49.86 &= q - 55.84 \\ q &= 5.98 \text{ kJ/mol} \end{aligned}$$

5. (b)

$$\begin{aligned} \text{Ca(OH)}_2 + 2\text{HNO}_3 &\longrightarrow \text{Ca(NO}_3)_2 + 2\text{H}_2\text{O} \\ \Delta H &= 2 \times \Delta H_{\text{neutralisation}} \\ &= 2 \times (-55.84) \\ &= -111.68 \text{ kJ} \end{aligned}$$

6. (b)

$$\begin{aligned} \text{H}_2\text{SO}_4 + 2\text{NaOH} &\rightarrow \text{Na}_2\text{SO}_4 + 2\text{H}_2\text{O} \\ V_{\text{H}_2\text{SO}_4} &= V_1 \\ V_{\text{NaOH}} &= V_2 \\ V_1 + V_2 &= 100 \\ \text{For max temp rise} \\ 0.05V_1 \times 2 &= 0.1V_2 \\ V_1 = V_2 &= 50 \text{ ml} \end{aligned}$$

Passage - III

7. (c)

$$\begin{aligned} \Delta G &< 0 \text{ for spontaneous rxn} \\ \Delta H - T\Delta S &< 0 \\ \Delta S &> \frac{\Delta H}{T} \end{aligned}$$

$$\Delta S > \frac{15000}{300} = 50 \text{ J mole}^{-1} \text{K}^{-1}$$

8. (a)

$$\Delta G = \Delta H - T\Delta S$$

$$\Delta G = -T\Delta S$$

$$\Delta G = -T[-n_1 R \ln x_1 - n_2 R \ln x_2]$$

$$= 8.314 \times 298 \left[4 \ln \frac{4}{5} + 1 \ln \frac{1}{5} \right]$$

$$\Delta G = -6.19 \text{ kJ}$$

9. (a)

$$2\text{CoCl}_4(\text{aq}) + \text{Zn}(\text{s}) \rightarrow 2\text{CoCl}_3(\text{aq}) + \text{ZnCl}_2(\text{aq})$$

$$E = 0.4108 + 0.003T$$

$$\Delta S = -\frac{\partial(\Delta G)}{\partial T}$$

$$\Delta S = -\frac{\partial(-nFE)}{\partial T}$$

$$\Delta S = nF \frac{\partial E}{\partial T}$$

$$\Delta S = nF \times 0.003$$

$$\Delta S = 2 \times 96500 \times 0.003 = 579 \text{ JK}^{-1}$$

Passage - IV

10. (b)
11. (c)
12. (a)
13. (c)

Passage - V

14. (b)
15. (d)
16. (a)

Matching Type

1. (A) – P; (B) – S; (C) – R; (D) – Q
(A) Reversible cooling at constant volume
 $\Delta V = 0$
 $w = 0$
 $T_2 < T_1$
 $\Delta U < 0$
 $\Delta U = q < 0$ (P)

(B) Reversible isothermal expansion

$$\Delta T = 0 \Rightarrow \Delta U = 0$$

$$V_2 > V_1 \Rightarrow w < 0 \Rightarrow q > 0 \quad (S)$$

(C) Adiabatic expansion in vacuum $q = 0$

$$q = 0$$

$$P_{\text{ext}} = 0$$

$$V_2 > V_1, \quad w = 0 \Rightarrow \Delta U = 0 \quad (R)$$

(D) Reversible melting of sulphur at normal melting points heat required $\Rightarrow q > 0$

$$v_2 > v_1 \Rightarrow w < 0$$

$$\Delta U = q + w$$

$$q > w$$

$$\Delta V > 0$$

(Q)

2. (A) – PS; (B) – QR; (C) – R; (D) – S

(A) Reversible isothermal expansion

$$W = -nRT \ln \frac{V_2}{V_1} = -2.303nRT \log \frac{V_2}{V_1} \quad (\text{only for isothermal reversible})$$

(P, S)

(B) Reversible adiabatic expansion

$$PV^\gamma = \text{constant} \quad (\text{only for reversible adiabatic})$$

$$W = \frac{nR}{\gamma - 1} (T_2 - T_1)$$

(Q, R)

(C) Irreversible adiabatic expansion

$$W = \Delta U = \frac{nR}{\gamma - 1} (T_2 - T_1) \quad (R)$$

(D) Irreversible isothermal compression $\Delta T = 0 \Rightarrow \Delta H = 0$

3. (A) – PS; (B) – R; (C) – Q; (D) – Q

(A) $(\Delta G_{\text{sus}})_{T,P} = 0$ equilibrium ΔG is useful work & here it is zero.

(P, S)

(B) $\Delta S_{\text{total}} > 0$

Spontaneous

(R)

(C) $\Delta S_{\text{total}} < 0$

Non-spontaneous

(Q)

(D) $(\Delta G_{\text{sus}})_{T,P} > 0$ non-spontaneous

(Q)

4. (A) – P; (B) – R, C – QS; (D) – Q
 (A) Heating of an ideal gas at constant pressure
 $\Delta T \neq 0 \Rightarrow \Delta H = nc_p \Delta T$
 (P)
 (B) Compression of liquid at constant temperature
 $\Delta U \neq nc \Delta T$ $\Delta G = V \Delta P + s \Delta T$
 (R)
 (C) Reversible process for an ideal gas at constant T
 $\Delta T = 0 \Rightarrow \Delta U = nq \Delta T = 0$
 $\Delta G = nRT \ln \frac{P_2}{P_1}$
 (Q,S)
 (D) Adiabatic free expansion of an ideal gas
 $w = -p_{\text{ext}} \Delta V = 0$
 $q = 0$
 $\Delta U = 0$
 (Q)
5. (A) – Q; (B) – P; (C) – R; (D) – S
 (A) $\Delta U = nc_v \Delta T$
 $\left(\frac{\partial U}{\partial T} \right)_v = C_v$ for 1 mole
 (Q)
 (B) $\Delta H = nc_p \Delta T$
 $\left(\frac{\partial H}{\partial T} \right)_p = C_p$ for 1 mole
 (C) $G = VdP - SdT$ at constant p
 $\left(\frac{\partial G}{\partial T} \right)_p = -S$
 (R)
 (D) $\partial G = vdp = sdT$ at constant T
 $\left(\frac{\partial G}{\partial p} \right)_T = V$

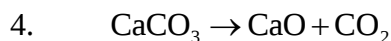
EXERCISE - 2 [C]

1. $W = -nRT \ln \frac{V_f}{V_i}$
 $= 1 \times 8.314 \times 298 \ln \left(\frac{1}{5} \right) = -3.988 \text{ kJ}$
2. $V = 0.5 \text{ lt} \longrightarrow 4 \text{ lt}$
 $T = 298 \text{ K}$
 $TV^{\gamma-1} = \text{constant}$

$$298 \times (0.5)^{1/3} = T \times 4^{1/3}$$

$$\text{So, } T = 149\text{K}$$

$$3. \quad \Delta E = q + W = (-65) + (+20) = -45\text{J}$$



$$q = \Delta H = 177.9\text{kJ}$$

$$\Delta H = \Delta E + P\Delta V$$

$$\Delta U = 177.9 - \left(24.4 + \frac{16.9}{1000} - \frac{34.2}{1000} \right) \times 0.101325 = 175.4\text{ kJ}$$

$$5. \quad \begin{array}{ccc} n=1 & & n=1 \\ 300\text{ K} & & T \\ 10\text{ atm} & \xrightarrow{\gamma=1.33} & 1\text{ atm} \\ V_1 & & V_2 \end{array}$$

$$q = 0$$

$$\Delta E = W$$

$$\Rightarrow -1 \times \left(\frac{1 \times R \times T}{1} - \frac{1 \times R \times 300}{10} \right) = 1 \times 3R \times (T - 300)$$

$$= -(T - 30) = 3(T - 300)$$

$$= 4T = 930$$

$$\Rightarrow T = 232.5$$

$$\Rightarrow \Delta E = W = nC_V \Delta T = 1 \times 3 \times 8.314 \times (232.5 - 300)$$

$$\Rightarrow \boxed{W = -1.683\text{kJ}}$$

$$6. \quad TV^{\gamma-1} = k$$

$$300 V^{1/3} = T \times (27V)^{1/3}$$

$$\Rightarrow \boxed{100\text{K} = T}$$

$$\Delta E = W = 1 \times 25.08 \times (100 - 300) = 5016$$

$$7. \quad TV^{\gamma-1} = k$$

$$298.15 \times V^{\gamma-1} = 248.44 \times (2V)^{\gamma-1}$$

$$\frac{298.15}{248.44} = (2)^{\gamma-1}$$

$$\log \left(\frac{298.15}{248.44} \right) = (\gamma - 1) \log 2$$

$$\gamma - 1 = 0.263$$

$$C_V = 31.61$$

$$8. \quad W = -1 \times \left(\frac{298R}{1} - \frac{298R}{5} \right) = -19.57\text{ L-atm}$$

9. $T_A = \frac{1 \times 22.4}{0.082} = 273 \text{ K}$
 $T_B = \frac{1 \times 44.8}{0.082} = 546 \text{ K}$
 $T_C = \frac{0.5 \times 44.8}{0.082} = 273 \text{ K}$
 For process $\vec{A}$
 $\Delta E = 1 \times \frac{3}{2} \times R \times 273 = 3.4 \text{ kJ}$
 $q = \Delta H = 1 \times \frac{5}{2} \times R \times 273 = 5.67 \text{ kJ}$
 $W = \Delta E - q = -R \times 273 = -2.27 \text{ kJ}$
 For process $\vec{B}$
 $W = 0$
 $q = \Delta E = 1 \times \frac{3}{2} R \times (-273) = -3.4 \text{ kJ}$
 For process $\vec{C}$
 $\Delta E = \Delta H = 0$
 $W = (-q) = -1 \times 8.314 \times 273 \ln \frac{22.4}{44.8}$
 $= -8.314 \times 273 \ln \frac{1}{2}$
 $= +8.314 \times 273 \times \ln 2$
 $= 1572.9 \text{ J}$
10. $q = \Delta H$ (constant pressure process)
 $\Rightarrow \Delta H = +1 \text{ kcal}$
 $\therefore \Delta H = \Delta E + P\Delta V$
 $\Rightarrow \Delta E = 1 \text{ kcal} - \frac{(1 \times 0.3) \times 0.101325}{4.2} = 0.993 \text{ kcal}$
11. $\Delta H = 1440 \text{ cal}$
 $\therefore \Delta H = \Delta E + P\Delta V$
 $\therefore \Delta H = \Delta E + 1 \times (0.018 - 0.0196)$
 $\Rightarrow \Delta E = 1440 \text{ cal} - 101.325 \times \frac{-0.0016 \times 1}{4.2}$
 $= 1440 + 0.0386 \text{ cal}$
 ≈ 1440
12. $W = -1 \times (1.1 - 1)$
 $\Rightarrow -0.1 \text{ L-atm} = -10.1325 \text{ J}$
13. $q = \Delta H = -36.5 \text{ kJ}$
 $W = \frac{-1 \times 500 \text{ cm}^2 \times 50 \text{ cm}}{1000} = -25 \text{ L-atm} = -2.53 \text{ kJ}$

$$\Delta H = \Delta E + P\Delta V$$

$$\Delta E = -36.5 \text{ kJ} - 2.53 \text{ kJ}$$

$$\approx -39.03 \text{ kJ}$$

14. $-P_{\text{ext}}(V_f - V_i) = nC_V(T_f - T_i)$

$$-1\left(\frac{nRT_f}{2} - \frac{nRT_i}{5}\right) = n \times \frac{5}{2}R(T_f - T_i)$$

$$3T_f = 2.7 T_i$$

$$T_f = 0.9 \times 300 = 270 \text{ K}$$

$$\Rightarrow \Delta E = W = 2 \times \frac{5}{2}R \times (270 - 300) = -1247.1$$

$$\Delta H = 2 \times \frac{7}{2}R \times (270 - 300) = -1745.9 \text{ J}$$

15. $P_{\text{ext}} = 1 \text{ atm}$

$$V_i = \frac{5 \times 0.082 \times 300}{4} = 30.75 \text{ L}$$

$$V_f = \frac{5 \times 0.082 \times 300}{1} = 123 \text{ L}$$

$$\therefore W = -1 \times (123 - 30.75) \times 101.325 \text{ J}$$

$$W = -9347 \text{ J}$$

Reversible

$$W = -5 \times 8.314 \times 300 \ln\left(\frac{4}{1}\right)$$

$$W = -17.288 \text{ kJ}$$

16. $n = 3$

$$T = 200 \text{ K} \xrightarrow[\text{adiabatic}]{\text{reversible}} T = 250 \text{ K}$$

$$P = 2 \text{ atm} \qquad P$$

$$V_1 \qquad V_2$$

$$C_V = 27.5$$

$$\Rightarrow 2 \times V_1 = 3 \times 0.082 \times 200$$

$$V_1 = 3 \times 0.082 \times 100$$

$$V_1 = 0.246 \times 100 = 24.6 \text{ L}$$

$$q = 0 \qquad W = \Delta E = nC_V\Delta T = 3 \times 27.5 \times (250 - 200) = 4.125 \text{ kJ}$$

$$\Delta H = 3 \times (27.5 + 8.314) \times 50 = 5.372 \text{ kJ}$$

$$TV^{\gamma-1} = C$$

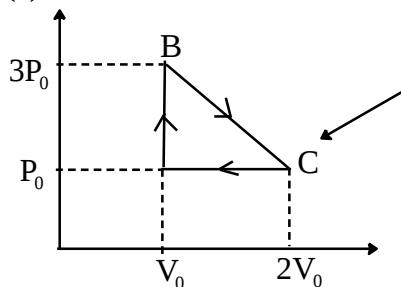
$$\gamma = \frac{C_P}{C_V} = \frac{35.814}{27.5} = 1.3$$

$$\Rightarrow 200 \times (24.6)^{0.3} = 250 \times (V_2)^{0.3}$$

$$\left(\frac{200}{250}\right)^{\frac{10}{3}} \times 24.6 = V_2 \Rightarrow V_2 = 11.7 \text{ L}$$

$$P = \frac{3 \times 0.082 \times 250}{11.7} = 5.256 \text{ atm}$$

17. (a)



$$n = 1$$

$$W = \frac{-1}{2} \times V_0 \times 2P_0$$

$$W = -P_0 V_0$$

$$\text{Workdone by the gas} = P_0 V_0$$

(b) $\overrightarrow{CA}$

$$W = P_0 \times V_0$$

$$\Delta E = 1 \times \frac{3}{2} R \times \left[\frac{P_0 V_0}{R} - \frac{2P_0 V_0}{R} \right]$$

$$\Delta E = \frac{3}{2} \times -P_0 V_0 = -\frac{3}{2} P_0 V_0 \quad \Delta E = q + W$$

$$\Rightarrow q = -\frac{3}{2} P_0 V_0 - P_0 V_0$$

$$q = -\frac{5}{2} P_0 V_0$$

$\overrightarrow{AB}$

$$W = 0$$

$$\Delta W = 1 \times \frac{3R}{2} \times \left(\frac{3P_0 V_0}{R} - \frac{P_0 V_0}{R} \right)$$

$$\Delta E = 3P_0 V_0$$

(c) $\Delta U_{\text{total}} = q_{\text{total}} + W_{\text{total}}$

$$0 = (3P_0 V_0 + Q_{BC} - 2.5P_0 V_0) - P_0 V_0$$

$$Q_{BC} = 0.5P_0 V_0$$

(d) $\frac{y - 3P_0}{x - V_0} = \frac{3P_0 - P_0}{V_0 - 2V_0}$

$$\frac{P - 3P_0}{V - V_0} = \frac{2P_0}{-V_0}$$

$$P = 5P_0 - \frac{2P_0}{V_0} V$$

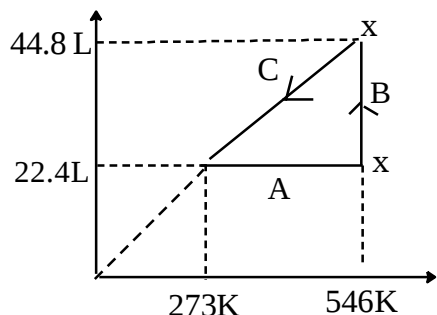
$$T = \frac{5P_0}{R}V - \frac{2P_0}{RV_0}V^2$$

$$\frac{dT}{dV} = \frac{5P_0}{R} - \frac{4P_0}{RV_0}V = 0$$

$$\Rightarrow V = \frac{5V_0}{4}$$

$$T_{\max} = \frac{5P_0}{R} \left(\frac{5V_0}{4} \right) - \frac{2P_0}{RV_0} \left(\frac{5V_0}{4} \right)^2 = \frac{25}{8} P_0 V_0 / R$$

18.



$$P_1 = 1 \times \frac{0.082 \times 273}{22.4} = 1 \text{ atm}$$

$$P_2 = 1 \times \frac{0.082 \times 546}{22.4} = 2 \text{ atm}$$

$$P_3 = 1 \times \frac{0.082 \times 546}{44.8} = 1 \text{ atm}$$

A is isochoric

$$W = 0$$

$$q = \Delta E = 1 \times \frac{3}{2} \times 8.314 \times (546 - 273) = 3404.583 \text{ J}$$

$$\Delta H = 1 \times \frac{5}{2} \times 8.314 \times (546 - 273)$$

B is isothermal

$$\Rightarrow \Delta E = \Delta H = 0 \quad \Delta E = q + W$$

$$W = -q = -1 \times R \times 546 \text{ K} \left(\frac{44.8}{22.4} \right) = -R \ln 2 \times 546$$

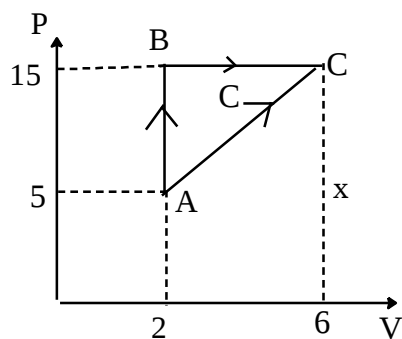
C is isobaric

$$\Delta E = 1 \times \frac{3}{2} \times R \times (-273) \quad \Delta E = q + W$$

$$\Delta H = 1 \times \frac{5}{2} \times R \times (-273) \quad -\frac{3}{2} R 273 = -\frac{5}{2} R \times 273 + W$$

$$Q = \Delta H = 1 \times \frac{5}{2} \times R \times 273 \quad W = R \times 273$$

19. Area under the curve AC is less than W is less for process AC.



(b) $q_{AC} = +200\text{J}$

$$W = \frac{1}{2} \times (5 + 15) \times 4$$

$$= \frac{1}{2} \times 20 \times 4 = 40\text{J}$$

$$W = -40\text{J}$$

$$\therefore \Delta E = q + W$$

$$\Rightarrow E_C - E_A = +200 - 40$$

$$\Rightarrow E_C = 160 + 10 = 170\text{J}$$

(c) $\omega_{AB} = 0$

$$q = \Delta E$$

$$\Rightarrow q = 10\text{J}$$

20. $\Delta H = \Delta E + \Delta nRT$

$$= -14.2\text{kcal/mol} + \frac{1 \times 2 \times 298}{1000}$$

$$= (-14.2 + 0.6)\text{kcal}$$

$$= -13.6\text{kcal}$$

21. $q = nc\Delta T$

$$= \frac{213.5}{18} \times 18 \times 75$$

$$= 16.012\text{kcal}$$

22. $V_1 = 3\text{dm}^3 \longrightarrow 5.0\text{dm}^3$

$$P_{\text{net}} = 3\text{atm}$$

$$\Rightarrow \omega = -3 \times 2\text{atm} \approx -6 \times 100\text{J}$$

$$q = \omega \therefore q = mc\Delta T (\because C \text{ in } g^{-1})$$

$$\Rightarrow 6 \times 100 = 180 \times 4.18 (\Delta T)$$

$$0.8 \sim \Delta T$$

$$\Rightarrow T - 290 = 0.8$$

$$\Rightarrow T = 290.8\text{K}$$

23. P is constant
 (a) So, $Q = \Delta H = 22.2 \text{ kJ}$
 (b) $\Delta H_v = \frac{22.2}{10/18} = 39.96 \text{ kJ / mole}$
 (c) $W = -(n_g)RT$
 $= -\frac{10}{18} \times 8.314 \times 373$
 $= -1722.85 \text{ J}$
 $= -1.72 \text{ kJ}$
 (d) $\Delta E = Q + W$
 $= 22.2 - 1.72$
 $= 20.48 \text{ kJ}$

24. $0.4 = 1 - \frac{T_C}{T_H}$
 $0.55 = 1 - \frac{T_C - 60}{T_H}$
 $0.55 = 1 - \frac{T_C}{T_H} + \frac{60}{T_H}$
 $0.15 = \frac{60}{T_H}$
 $T_H = \frac{60}{0.15} = 400$
 $T_C = 240$

25. $\Delta S = \frac{\Delta H}{T} \Rightarrow 29.4 = \frac{4.60 \times 10^3}{T}$
 $\Rightarrow T \approx 156.5 \text{ K}$

26. $\sum \frac{dq_{\text{rev}}}{T} = \sum ds$
 Since S is a state function cycle integral will be Zero.

27. $28.8 = \frac{30.5 \times 10^3}{T}$
 $\Rightarrow T = 1059 \text{ K}$

28. $dS = \int \frac{dQ}{T}$
 $dS = \int \frac{C_p dT}{T}$
 $= \int \frac{25.5}{T} dT + \int 13.6 \times 10^{-3} dT - \int 42.5 \times 10^{-7} T dT$
 $= 25.5 [\ln T]_{300}^{600} + 13.6 \times 10^{-3} (600 - 300)$

$$\begin{aligned}
 & -42.5 \times 10^{-7} \times \left[\frac{T^2}{2} \right]_{300}^{600} \\
 & = 25.5 \ln 2 + 13.6 \times 10^{-3} \times 300 - \frac{42.5 \times 10^{-7}}{2} \times (600^2 - 360^2) \\
 & = 17.67 + 4.08 - \frac{42.5}{2} \times 10^{-7} \times 6^2 - 3^2 \times 10^4 \\
 & = 17.67 + 4.08 - 573 - 75 \times 10^{-3} \\
 & = 21.177 \text{ JK}^{-1} \text{ mol}^{-1}
 \end{aligned}$$

29. $\Delta S = 2 \times 239.7 - (152.3 + 223)$
 $= 479.4 - 375.3$
 $= 104.1 \text{ J / mol}^{-1} \text{ K}$
 $\Delta G = 29300 - 298 \times 104.1$
 $= -1721.8$

30. $\Delta G = \Delta H - T\Delta S$
 $= -2808 \times 10^3 - 310 \times 182.4$
 $= -2864.5 \text{ kJ}$

31. $\text{Na(s)} + \frac{1}{2} \text{Cl}_2(\text{g}) \rightarrow \text{NaCl(s)}$
 $\Delta S = 72 - \left[51 + \frac{223}{2} \right] = -90.5 \text{ JK}^{-1} \text{ mol}^{-1}$
 $\frac{1}{2} \text{N}_2 - 2\text{H}_2 + \frac{1}{2} \text{Cl}_2 \longrightarrow \text{NH}_4\text{Cl(s)}$
 $\Delta S = 95 - \left[\frac{1}{2} \times 192 + 2 \times 131 + \frac{1}{2} \times 223 \right]$
 $= 95 - (96 + 262 + 111.5)$
 $= 95 - 419.5$
 $= -374.5 \text{ JK}^{-1} \text{ mol}^{-1}$
 Graphite $\rightarrow$ Diamond
 $\Rightarrow \Delta S = -[5.19 - 2.43] = -3.26 \text{ JK}^{-1} \text{ mol}^{-1}$

32. $\Delta H = -106.7 - (-139.3) = 32.6 \text{ kJ / mol}$
 $\Delta G = 32.6 \times 10^3 - 298 \times 94.98$
 $= 32600 - 28304$
 $= +ve$

33. $\text{CO(g)} + \frac{1}{2} \text{O}_2(\text{g}) \longrightarrow \text{CO}_2(\text{g})$
 $\Delta H^\circ = -393.5 - [-110.5 + 0]$
 $\Delta H^\circ = -283 \text{ kJ / mol}$

$$\Delta S^\circ = 213.7 - \left[197.6 + \frac{205}{2} \right]$$

$$\Delta S^\circ = -86.4 \text{ JK}^{-1}\text{mol}$$

$$\Delta G^\circ = -283000 - 298 \times (-86.4)$$

$$\Delta G^\circ = -257.25 \text{ kJ}$$

34. $\Delta H = \Delta E + (-1) \times 8.314 \times 298$

$$\Delta H = -10.46 - \frac{2477.5}{1000}$$

$$= -12.9375$$

$$\Delta G = -12.94 \times 10^3 - 298 \times (-43.93)$$

$$= 151 \text{ J}$$

$$= +0.151 \text{ kJ mol}^{-1}$$

Not feasible.



(I) $\Delta H = -94.05 - [-57.8 - 26.42] = -9.83 \text{ kcal}$

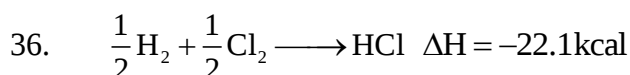
(II) $\Delta G = 0 + (-94.24) - [-54.64 - 32.79]$
 $= -6.81 \text{ kcal / mol}$

(III) $-6.81 \times 10^3 = -9.83 \times 10^3 - 298 \times \Delta S$
 $\Rightarrow \Delta S = -10.13 \text{ cal}$

(IV) $\Delta H = \Delta E (\because \Delta n = 0)$

$$\Delta E = -9.83 \text{ kcal / mol}$$

(V) $\Delta S = 31.2 + 81.1 - [x + 47.3] = -10.13 = +45.13 \text{ cal mol}^{-1} \text{ K}^{-1}$



$$\frac{\Delta H_{350} - \Delta H_{300}}{350 - 300} = 1 \times 6.8 - \left[\frac{6.82}{2} + \frac{7.7}{2} \right]$$

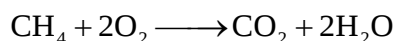
$$\frac{\Delta H_{350} - 22.1 \text{ kcal}}{50} = \frac{6.8 - 7.26}{1000} = -\frac{0.46}{1000}$$

$$\Delta H_{350} + 22.1 \text{ kcal} = -\frac{23}{1000}$$

$$\Rightarrow \Delta H_{350} = -22.123 \text{ kcal}$$

37. $1 \text{ m}^3 = 1000 \ell$

$$\Rightarrow 1000 \ell = \frac{1000}{22.7} \text{ mole}$$



$$\Delta H = -2 \times 241.6 - 398.8 - (-76.2)$$

$$= -805.8 \text{ kJ / mol}$$

$$\therefore \text{Heat evolved} = \frac{1000}{22.7} \times 805.8 \text{ kJ/mol}$$

$$= 35.498 \text{ MJ}$$

38. $\text{C}_2\text{H}_6 + \frac{7}{2}\text{O}_2 \longrightarrow 2\text{CO}_2 + 3\text{H}_2\text{O}$

$$\Delta H = -\frac{3120}{2}$$

$$\Rightarrow -\frac{3120}{2} = [2 \times -395 + 3 \times -286] - \Delta H_f^\circ(\text{C}_2\text{H}_6)$$

$$\Delta H_f^\circ(\text{C}_2\text{H}_6) = -(790 + 858) + \frac{3120}{2}$$

$$= -1648 + 1560$$

$$= -88 \text{ kJ/mol}$$

39. $\text{C(s)} + 2\text{S(standard)} \longrightarrow \text{CS}_2$

$$\Rightarrow \Delta H_f = +108.76 + [-393.3 + 2 \times -293.72]$$

$$= +108.76 - [393.3 + 2 \times 293.72]$$

$$= +128.02 \text{ kJ}$$

40. $\text{HgO(s)} \longrightarrow \text{Hg(s)} + \frac{1}{2}\text{O}_2(\text{g})$

$$\Delta H_R = 0 - (-90.8 \text{ kJ mol}^{-1})$$

$$= +90.8 \text{ kJ/mol}$$

$$1 \text{ mole HgO} \longrightarrow 90.8 \text{ kJ}$$

$$n_{\text{Hg}} = \frac{41.84}{90.8} = 0.461$$

$$m_{\text{Hg}} = 0.465 \times 200.6 = 92.44$$

$$\therefore \Delta H = \Delta E + \Delta nRT$$

$$90.8 = \Delta E + \frac{1}{2} \times \frac{8.314 \times 298}{1000}$$

$$90.8 \text{ kJ} = \Delta E + 1.24 \text{ kJ}$$

$$89.56 \text{ kJ} = \Delta E \quad \Rightarrow 89.56 \text{ kJ} \longrightarrow 1 \text{ mole Hg}$$

$$n_{\text{Hg}} = \frac{41.84}{89.56} = 0.4672$$

$$m_{\text{Hg}} = 0.4672 \times 200.6 = 93.72$$

41. $\text{C}_2\text{H}_4(\text{g}) + \text{H}_2(\text{g}) \longrightarrow \text{C}_2\text{H}_6$

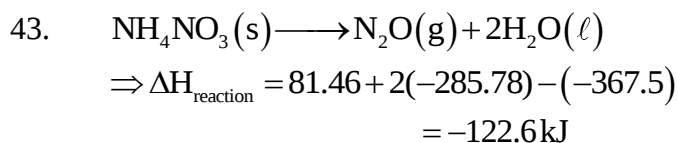
$$\Rightarrow \Delta H = -1410.8 - 285.9 + 1558.8$$

$$\Delta H = -136.9 \text{ kJ}$$

42. 14 kg of butane

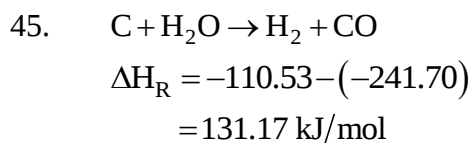
$$1 \text{ mole butane} \longrightarrow 2658 \text{ kJ heat}$$

$$\begin{aligned}
 1\text{ day} &\longrightarrow 20 \times 10^6 \text{ J} \\
 26\text{ day} &\longrightarrow 26 \times 2 \times 10^7 \text{ J} = 52 \times 10^7 \text{ J} \\
 &520,000 \text{ kJ} \\
 \Rightarrow 58\text{ g} &\longrightarrow 2658 \text{ kJ} \\
 14000\text{ g} &\longrightarrow \frac{2658}{58} \times 14000 \text{ kJ} \\
 &641,586.2 \text{ kJ} \\
 \Delta &= 121586 \\
 = \% &= \frac{121586}{641586} \times 100 \\
 &= 18.95\%
 \end{aligned}$$

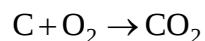


$$\Delta E = -122.6 - 1 \times \frac{8.314}{1000} \times 298 = -125.08 \text{ kJ}$$

44. $\Delta H = -337 - 68.4 - (-373)$
 $= -32.4 \text{ kcal}$



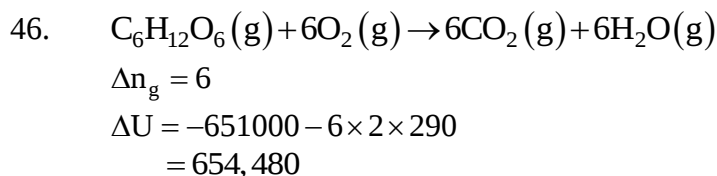
$$\text{So, total heat required} = 131.17 \times \frac{100}{12}$$



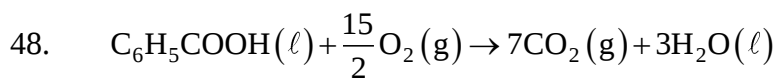
$$\Delta H_{\text{R}} = -393.51 \text{ kJ / mole}$$

$$131.17 \times \frac{100}{12} = 393.51 \times \frac{x}{12}$$

$$\Rightarrow x = \frac{100}{3} = 33.33 \text{ g}$$



47. $n_{\text{CH}_4} = \frac{89.03}{890.3} = \frac{1}{10} \Rightarrow W_{\text{CH}_4} = 1.6 \text{ g}$
 $n_{\text{CO}_2} = \frac{89.03}{890.3} = \frac{1}{10} \Rightarrow W_{\text{CO}_2} = 4.4 \text{ g}$



$$\Delta U_{\text{R}} = -\frac{23.85 \times 0.55}{\frac{0.5}{122}} = -3200.67$$

$$\Delta H_{\text{R}} = -3200.67 + \left(-\frac{1}{2} \times \frac{8.314}{1000} \times 288 \right) = -3201.87$$

$$49. \quad \frac{120}{180} \times 2880 \times \frac{1}{4} = 100 \times x$$

$$x = 4.8$$

$$50. \quad \Delta_{\text{R}} C_{\text{P}} = 2 \times 4\text{R} - \frac{7}{2}\text{R} - 3 \times \frac{7}{2}\text{R} = -6\text{R}$$

$$\Delta H_{323\text{K}} = \Delta H_{300\text{K}} + \int_{300}^{323} -6\text{R} dT$$

$$= -91.94 - \frac{6 \times 8.31 \times 23}{1000} = -93.09$$

$$51. \quad \Delta_{\text{R}} C_{\text{P}} = \left(\frac{8}{5}\alpha + 4\beta T \right) - 3 \times (\alpha + \beta T) = -\frac{7}{5}\alpha + \beta T$$

$$\Delta H_{600\text{K}} = \Delta H_{300\text{K}} + \frac{1}{1000} \int_{300}^{600} \left(-\frac{7}{5}\alpha + \beta T \right) dT$$

$$= -100 - \frac{7}{5}\alpha \times \frac{300}{1000} + \frac{\beta}{2000} (600^2 - 300^2)$$

$$= -100 - 0.42\alpha + 135\beta$$

$$52. \quad \Delta H_{\text{C, Propene}} = 3 \times (-393.5 - 285.8) - 20.42 = -2058.32$$

$$\Delta H_{\text{C, Cyclopropene}} = -2058.32 - 33 = -2091.32$$

$$53. \quad (1) + (2) - (3)$$

$$\Delta H_{\text{f}} = -48 - 68.4 + 14 = -102.4$$

$$54. \quad \Delta_{\text{R}} C_{\text{P}} = \left(7.3 + \frac{3}{100} T \right) - \left(7.3 + \frac{2}{100} T \right) = \frac{T}{100}$$

$$\Delta H_{1000\text{K}} = \Delta H_{300\text{K}} + \frac{1}{1000} \int_{300}^{1000} \frac{T}{100} \times dT$$

$$= -41.8 + \frac{1}{1000} \times \frac{1000^2 - 300^2}{200} = -37.25 \text{ kJ}$$

$$55. \quad -105 = 20.5 + 96 + 28.75 + x - 159.5$$

$$x = -90.75 \text{ kcal/mole}$$

56. Delong and petit law
 $0.0276 \times \text{At.wt} \approx 6.4$
 $\Rightarrow \text{At.wt} \approx 232$
 $\frac{79.34}{\frac{232}{x}} = \frac{114.79 - 79.34}{35.5} \Rightarrow x = 2.92$
 So, exact value of x is 3.
 $\frac{79.34}{\frac{\text{AW}}{3}} = \frac{114.79 - 79.34}{35.5} \Rightarrow \text{AW} = 238.36$
57. $\text{C}_2\text{H}_2 + \frac{5}{2}\text{O}_2 \rightarrow 2\text{CO}_2 + \text{H}_2\text{O}$
 $\Delta H = -312 = 2 \times (-94.38) + (-68.38) - \Delta H_{f, \text{C}_2\text{H}_2}$
 $\Delta H_{f, \text{C}_2\text{H}_2} = 54.86$
 $2\text{C} + \text{H}_2 \rightarrow \text{C}_2\text{H}_2$
 $\Delta H = 54.86 = 2 \times 150 + 2 \times 51.5 - 2 \times 93.6 - \text{BE}_{\text{C}\equiv\text{C}}$
 $\text{BE}_{\text{C}\equiv\text{C}} = 160.94$
58. $\text{CuSO}_4 + 5\text{H}_2\text{O} \longrightarrow \text{CuSO}_4 \cdot 5\text{H}_2\text{O}$
 $\Delta H = -15.9 - 2.8 = -18.7$
59. $\text{HAuBr}_4 + 4\text{HCl} \rightarrow \text{HAuCl}_4 + 4\text{HBr}$
 $\Delta H_R = 36.8 - 28 = 8.8 \text{ kcal/mole}$
 $n_{\text{HAuBr}_4} = \frac{0.44}{8.8} = \frac{1}{20}$
 $\% \text{ conversion} = \frac{1}{20} \times 100 = 5\%$
60. (i) – (ii)
 1-Butene $\rightarrow$ trans-2-butene
 $\Delta H = \Delta H_1 - \Delta H_2 = -649.8 + 647 = -2.8$
 So, $\Delta H_1 = -1$, $\Delta H_2 = 1.8$
61. $\Delta H_R = (35.5 + 3 \times 414 + 351.5 + 464.5) + \left(\frac{3}{2} \times 494\right) - (2 \times 711 + 143) - (2 \times 40.6 + 4 \times 464.5)$
 $= -669.7 \text{ kJ}$

Only One Option Correct

1. (b)

2. (a)

3. (c)

4. (b)

5. (c)

6. (a)

7. (d)

8. (d)

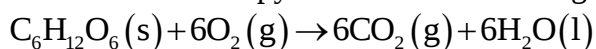
9. (a)

10. (b)

11. (a)

12. (c)

The standard enthalpy of the combustion of glucose can be calculated by the equation



$$\Delta H_{\text{C}} = 6 \times \Delta H_{\text{f}}(\text{CO}_2) + 6 \times \Delta H_{\text{f}}(\text{H}_2\text{O}) - \Delta H_{\text{f}}(\text{C}_6\text{H}_{12}\text{O}_6)$$

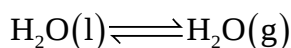
$$\Delta H^{\circ} = 6(-400) + 6(-300) - (-1300) = -2900 \text{ kJ/mol}$$

For one gram of glucose, enthalpy of combustion

$$\Delta H^{\circ} = -\frac{2900}{180} = -16.11 \text{ kJ/g}$$

13. (b)

Given conditions are boiling conditions for water due to which system is in equilibrium.



$$\Delta S_{\text{total}} = 0$$

$$\Delta S_{\text{system}} + \Delta S_{\text{surroundings}} = 0$$

$$\Delta S_{\text{system}} = -\Delta S_{\text{surroundings}}$$

For process, $\Delta S_{\text{system}} > 0$

$$\Delta S_{\text{surroundings}} < 0$$

14. (c)

From 1st law of thermodynamics

$$q_{\text{sys}} = \Delta U - w = 0 - [-P_{\text{ext}} \Delta V]$$

$$= 3.0 \text{ atm} \times (2.0 \text{ L} - 1.0 \text{ L}) = 3.0 \text{ L-atm}$$

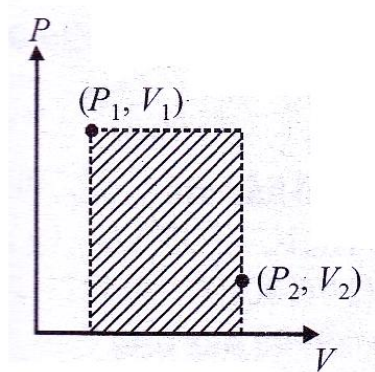
$$\therefore \Delta S_{\text{surr}} = \frac{(q_{\text{rev}})_{\text{surr}}}{T} = -\frac{q_{\text{sys}}}{T}$$

$$= -\frac{3.0 \times 101.3 \text{ J}}{300 \text{ K}} = -1.013 \text{ J/K}$$

15. (a)
 $\text{C}(\text{graphite}) \rightarrow \text{C}(\text{diamond})$ (Isothermally)
 $\Delta_r G^\circ = \Delta G^\circ(\text{diamond}) - \Delta G^\circ(\text{graphite})$
 $-2.9 \times 10^3 = -\Delta P \times 2 \times 10^{-6}$
 $\Delta P = \frac{2.9 \times 10^3}{2 \times 10^{-6}} = 1.45 \times 10^9 \text{ Pa} = 1.45 \times 10^9 \times 10^{-5} \text{ bar}$
 $= 1.45 \times 10^4 \text{ bar} = 14500 \text{ bar}$
 $P = \Delta P + P_0 = 14500 + 1 = 14501 \text{ bar}$

One or More than One Option Correct

1. (a, c, d **or** a, d)
 2. (a, c)
 3. (a, b, c)
 Since the vessel is thermally insulated, $q = 0$
 Further since, $P_{\text{ext}} = 0$, so $w = 0$, hence $\Delta U = 0$
 Therefore, $\Delta T = 0$, $T_2 = T_1$ and $P_2 V_2 = P_1 V_1$
 However, the process is adiabatic irreversible, so we can't apply $P_2 V_2^\gamma = P_1 V_1^\gamma$.
 4. (a, b, c)
 (a)



During irreversible compression, maximum work is done on the gas (corresponding to shaded area) when $P_1 = P_2$

- (d) When $T_1 = T_2 \Rightarrow \Delta U = nC_V \Delta T = 0$

In reversible adiabatic expansion, $T_2 < T_1$

$\therefore \Delta T = -\text{ve}$ and also $\Delta U = -\text{ve}$

- (B) In free expansion, $P_{\text{ext}} = 0$, $\therefore W = 0$

From 1st law of thermodynamics,

$$\Delta U = q + W$$

$$\therefore \Delta U = q$$

If expansion is carried out isothermally, $\Delta U = 0$

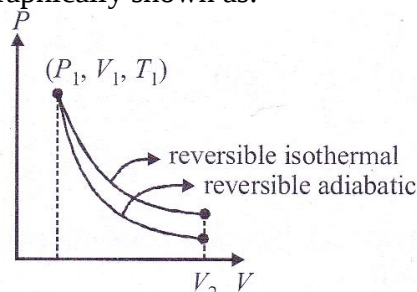
Hence $q = 0$

$\therefore$ It is adiabatic process.

If carried out adiabatically ($q = 0$) $\therefore \Delta U = 0$

$\therefore$ It is an isothermal process

(c) During adiabatic expansion, the final temperature is less than the initial temperature. Therefore, the final volume in adiabatic expansion will also be less than the final volume in isothermal expansion. This can be graphically shown as:



The magnitude of work done by the gas is equal to the area under the curve. As seen from the figure, the area under curve in reversible isothermal is more. Hence, the magnitude of work done is lesser in adiabatic reversible expansion as compared to the corresponding work in isothermal expansion.

5. (b, c)

A – C $\Rightarrow$ isochoric process

A – B $\Rightarrow$ isothermal process

B – C $\Rightarrow$ isobaric process

$$(a) \quad q_{AC} = \Delta U_{AC} = nC_{V,m}(T_2 - T_1) = \Delta U_{BC}$$

$$W_{AB} = -nRT \ln \left(\frac{V_2}{V_1} \right) \text{ (pressure is not constant)}$$

$$(b) \quad W_{BC} = -P_2(V_1 - V_2) = P_2(V_2 - V_1)$$

$$q_{BC} = \Delta H_{BC} = nC_{p,m}(T_2 - T_1) = \Delta H_{AC}$$

$$(c) \quad \Delta H_{CA} = nC_{p,m}(T_1 - T_2)$$

$$(d) \quad \Delta U_{CA} = nC_{V,m}(T_1 - T_2)$$

$$\Delta H_{CA} < \Delta U_{CA} \text{ since both are negative } (T_1 < T_2) \text{ and } C_{p,m} > C_{V,m}$$

6. (a, c)

Enthalpy of formation is the enthalpy change for formation of 1 mole of substance from its elements present in the most stable natural form.

7. (a, b, c)

P-V work done is applicable for reversible isobaric as well as isothermal and adiabatic process.

$$w = -\int P_{\text{ext}}.dV$$

For van der Waals equation

$$P_{\text{ext}} = P = \left(\frac{RT}{v-b} - \frac{a}{v^2} \right)$$

$$w = -\int dv \left(\frac{RT}{v-b} - \frac{a}{v^2} \right) \quad \dots\dots(i)$$

Equation (i) is not applicable to irreversible process. Therefore work done is calculated assuming pressure is constant throughout the process.

8. (a, b, d)
 From state I to II (Reversible isothermal expansion):
 $T \rightarrow \text{constant}, \Delta V \rightarrow +ve, \Delta S \rightarrow +ve, \Delta H \rightarrow 0$
 $\Delta P \rightarrow -ve$
 From state II to III (Reversible adiabatic expansion):
 $q \rightarrow 0, \Delta V \rightarrow +ve, \Delta S \rightarrow \text{constant}$
 $\Delta H \rightarrow -ve, \Delta P \rightarrow -ve, \Delta T \rightarrow -ve$
 $\therefore$ Plots (a), (b), (d) are correct while (c) is wrong as from state II to III, H is decreasing.

Paragraph Type

Passage - I

1. (c)
 $K \rightarrow L \Rightarrow V$ increasing at constant P
 Hence, T increases (Heating)
 $L \rightarrow M \Rightarrow P$ decreasing at constant V
 Hence, T decreases (Cooling),
 $M \rightarrow N \Rightarrow V$ decreasing at constant P
 Hence, T decreases (Cooling),
 $N \rightarrow K \Rightarrow P$ increasing at constant V
 Hence, T increases (Heating)
2. (b)
 L to M and N to K , both are having constant volume therefore, these processes are isochoric.

Numerical Value Answer

1. (935.00)
 $\text{SnO}_2(s) + \text{C}(s) \longrightarrow \text{Sn}(s) + \text{CO}_2(g)$
 $\Delta_f H^\circ = [-394] - [-581] = 187 \text{ kJ / mole} = 187 \times 10^3 \text{ J / mol}$
 $\Delta_f S^\circ = [52 + 210] - [56 + 6] = 200 \text{ JK}^{-1}\text{mol}^{-1}$
 $T = \frac{\Delta_f H^\circ}{\Delta_f S^\circ} = \frac{187 \times 10^3}{200} = 935 \text{ K}$
2. (10)
 Process (I) $\Rightarrow$ (Adiabatic reversible)
 $\frac{\Delta U}{R} = 450 - 2250$
 $\Delta U = -1800R$
 $W_1 = \Delta U = -1800R$
 Process(II) $\Rightarrow$ (Reversible isothermal process)
 $T_1 = 900\text{K}$
 Calculation of T_2 after reversible adiabatic process
 $\Delta U = nC_v dT$
 $\Rightarrow -1800R = 1 \frac{5}{2} R (T_2 - 900)$
 $T_2 = 180\text{K}$

$$W_{II} = -nRT_2 \ln \frac{V_3}{V_2} = W_I$$

$$\Rightarrow -1 \times R \times 180 \ln \frac{V_3}{V_2} = -1800R$$

$$\Rightarrow \ln \frac{V_3}{V_2} = 10$$

3. (166.28)

$$\text{Slope} = \frac{dy}{dx} = \frac{d(\ln K)}{d(10^4/T)}$$

$$\Rightarrow \frac{-\Delta H^\circ}{10^4 R} = \frac{-7 - (-3)}{12 - 10}$$

$$\Rightarrow \Delta H^\circ = 2 \times 10^4 \times 8.314 \text{ J/mol}$$

$$= 166.28 \text{ kJ/mol}$$

4. (141.34)

From the plot when, $\frac{10^4}{T} = 10$ [T = 1000K]

$$\ln \left(\frac{p_2}{1} \right) = -3$$

$$\Delta G^\circ = -RT \ln K \Rightarrow \Delta H^\circ - T\Delta S^\circ = -RT \ln \frac{p_z}{p^\circ}$$

Substituting in following equation:

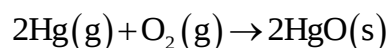
$$\ln \left(\frac{p_z}{1} \right) = -\frac{\Delta H^\circ}{RT} + \frac{\Delta S^\circ}{R}$$

$$\text{We get, } -3 = -\frac{2 \times 10^4 \times R}{R \times 1000} + \frac{\Delta S^\circ}{R}$$

$$\Rightarrow S^\circ = 17R \Rightarrow \Delta S^\circ = 17 \times 8.314 \text{ J/K-mol}$$

$$\Rightarrow \Delta S^\circ = 141.34 \text{ J/K-mol}$$

5. (90.39)



$$\Delta_r H^\circ = 2\Delta_f H^\circ(\text{HgO, s}) - 2\Delta_f H^\circ(\text{Hg, g}) - \Delta_f H^\circ(\text{O}_2, \text{g})$$

$$= 2\Delta_f H^\circ(\text{HgO, s}) - 2\Delta_f H^\circ(\text{Hg, g}) \quad \dots\dots\dots(i)$$

$$\left[\because \Delta_f H^\circ(\text{O}_2, \text{g}) = 0 \right]$$

Now, $\Delta_r H^\circ$ is the heat evolved by bomb calorimeter due to the occurrence of the reaction at constant volume.

$$\therefore -(Q_v)_r = \Delta_r U$$

$$\therefore \Delta_r H = \Delta_r U + \Delta n_g R = -C\Delta T + \Delta n_g RT$$

[Where C – the heat capacity of calorimeter = 20 kJ/K at 298K]

$$= -[20(312.8 - 298)] - 3RT$$

$$= -296 - 3 \times 8.3 \times 10^{-3} \times 298 \text{ kJ} = -303.42 \text{ kJ}$$

Hence, from equation (i)

$$-303.42 = 2\Delta_f H^\circ (\text{HgO}, s) - 2 \times 61.32$$

$$\text{Or, } 2\Delta_f H^\circ (\text{HgO}, s) = -180.78 \text{ kJ}$$

$\therefore$ Standard Molar Enthalpy of formation of HgO

$$= \frac{-180.78}{2} = -90.39 \text{ kJ}$$

$$\Rightarrow |X| = 90.39$$

6. (0.31)

S_T and S_0 are entropies of the phases at temperatures T and 0 K , respectively.

$$S = S_0 + \int C_p \frac{dT}{T} \quad [S_0 = 0 \text{ at } 0 \text{ K}]$$

$$\Rightarrow S_\alpha = S_0 + \int (C_p)_\alpha \frac{dT}{T}$$

$$\Rightarrow S_\beta = S_0 + \int (C_p)_\beta \frac{dT}{T}$$

$$\Rightarrow S_\beta - S_\alpha = \left[(C_p)_\beta - (C_p)_\alpha \right] \int \frac{dT}{T}$$

$$\text{Given, } C_{p\beta} - C_{p\alpha} = 1$$

$$S_\beta - S_\alpha = \ln T + C \text{ at any temperature } T.$$

$$\Rightarrow (S_\beta - S_\alpha)_{T_2} - (S_\beta - S_\alpha)_{T_1} = \ln T_2 - \ln T_1$$

$$T_2 = 600 \text{ K}, T_1 = 300 \text{ K, from the graph } S_\beta - S_\alpha \text{ at } 600^\circ\text{C} = 1$$

$$(1) - (S_\beta - S_\alpha)_{300} = \ln 600 - \ln 300$$

$$1 - (S_\beta - S_\alpha)_{300} = \ln 2 = 0.69$$

$$\Rightarrow (S_\beta - S_\alpha)_{300} = 1 - 0.69$$

$$= 0.31 \text{ J mol}^{-1} \text{K}^{-1}$$

7. (300)

Change in Gibbs free energy transition from α to β phase = 0

Thus, $\Delta H = T\Delta S$

$$\Delta H (\text{at } 600 \text{ K}) = 600 \times 1 \quad [\because \Delta S = 1]$$

$$= 600 \text{ J mol}^{-1}$$

According to Kirchhoff's law,

$$\Delta H_f - \Delta H_i = C_p (T_f - T_i) \quad \dots (i)$$

Using the Eq. (i),

$$\Delta H_{600} - \Delta H_{300} = 1 \times (C_{p,\beta} - C_{p,\alpha}) (600 - 300)$$

$$600 - \Delta H_{300} = 1 \times 1 \times 300$$

$$\Delta H_{300} = 600 - 300$$

$$= 300 \text{ J mol}^{-1}$$

8. (7)

A → B (reversible adiabatic)

$$\therefore T_1 V_1^{\gamma-1} = T_2 V_2^{\gamma-1}$$

$$T_1 = 600, V_1 = 10, T_2 = 60, \gamma = \frac{5}{3} \left(\text{from } C_{p,m} = \frac{5}{2} R \right)$$

$$\therefore (600)(10)^{2/3} = (60)(V_2)^{2/3}$$

$$(V_2)^{2/3} = (10)^{5/3}$$

$$\Rightarrow V_2 = (10)^{5/2}$$

Also, $q_{AB} = 0$ and $q_{AC} = RT_2 \ln 10$

$$\begin{aligned} \therefore q_{BC} &= nRT_2 \ln \left(\frac{V_3}{V_2} \right) \\ &= RT_2 \ln \left(\frac{V_3}{V_2} \right) \quad (\because n = 1) \end{aligned}$$

$$\Rightarrow q_{AC} = q_{BC}$$

$$\begin{aligned} \therefore \text{Total heat absorbed} \\ &= RT_2 \ln \left(\frac{V_3}{V_2} \right) = RT_2 \ln 10 \end{aligned}$$

$$\Rightarrow \ln \left(\frac{V_3}{V_2} \right) = \ln 10$$

$$V_3 = 10V_2$$

$$V_3 = 10(10)^{5/2} = (10)^{7/2}$$

Now, the value of

$$\begin{aligned} 2 \log V_3 &= 2 \log (10)^{7/2} \\ &= 2 \times \frac{7}{2} \log 10 = 7 \end{aligned}$$

9. (8120)

Given,

$$n = 5 \text{ mol}$$

$$C_{V,m} = 12 \text{ JK}^{-1} \text{ mol}^{-1}$$

$$R = 8.3 \text{ JK}^{-1} \text{ mol}^{-1}$$

$$T_2 = 415 \text{ K}$$

$$T_1 = 335 \text{ K}$$

$$V_2 = 20 \text{ L}$$

$$V_1 = 10 \text{ L}$$

Now, from the graph it is clear that X → Y is an isothermal process ($dT = 0$)

$$\text{So, } \Delta H_{X \rightarrow Y} = nC_p dT = 0$$

Also, Y → Z is an isochoric process

$$\Delta U_{Y \rightarrow Z} = nC_V dT$$

$$\Delta U_{Y \rightarrow Z} = 5 \times 12 \times (415 - 335)$$

$$\Delta U_{Y \rightarrow Z} = 4800 \text{ J}$$

$$\Delta H_{Y \rightarrow Z} = \Delta U_{Y \rightarrow Z} + \Delta(pV)$$

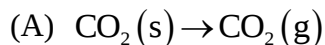
or $\Delta H_{Y \rightarrow Z} = \Delta U_{Y \rightarrow Z} + nR\Delta T$

$$\Delta H_{Y \rightarrow Z} = 4800 + (5 \times 8.3 \times 80)$$

$$\Delta H_{Y \rightarrow Z} = 8120 \text{ J}$$

Matrix-Match

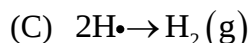
1. (A) – P, R, S ; (B) – R, S ; (C) – T ; (D) – P, Q, T



It is phase transition. The process is endothermic (sublimation). Gas is produced, so entropy increases.

- (B) On heating CaCO_3 decomposes. So, process is endothermic.

The energy increases as gaseous product is formed.



Entropy decrease as number of gaseous particle decreases.

- (D) The transition between different allotropes is considered as phase transition.

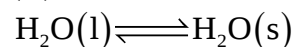
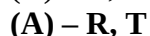
White and red P are allotropes.

Due to polymeric nature of red P, its entropy is less than that of white P.

Red P is more stable than white.

So, ΔH is –ve

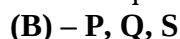
2. (A) – R, T ; (B) – P, Q, S ; (C) – P, Q, S ; (D) – P, Q, S, T



It is at equilibrium at 273 K and 1 atm

So, ΔS_{sys} is negative.

As it is equilibrium process, so $\Delta G = 0$



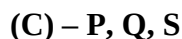
Expansion of 1 mole of an ideal in vacuum under isolated condition

Hence, $w = 0$

And $q_p = C_p dT (\because dT = 0)$

$\Rightarrow q = 0$

$\Delta U = C_v dT (\because dT = 0) \Delta U = 0$



Mixing of two ideal gases at constant temperature

Hence, $\Delta T = 0$

$\therefore q = 0; \Delta U = 0$

Also $w = 0 (\Delta U = q + w)$



Reversible heating and cooling of gas follows same path; also initial and final position is same.

Hence, $\left. \begin{matrix} q = 0 \\ w = 0 \end{matrix} \right\} \text{Path same}$

$\left. \begin{matrix} \Delta U = 0 \\ \Delta G = 0 \end{matrix} \right\} \text{State function}$

Subjective

1. $\Delta H = -114.52 \text{ J}$
2. $\Delta H^\circ = -285.4 \text{ kJ/mol}$, $\Delta G^\circ = -257.2 \text{ kJ/mol}$
3. (ii) $-W = q = 620.77 \text{ J}$, (iii) $\Delta H = 0$, $\Delta U = 0$, $\Delta S = 0$
4. $\Delta U = 0.1 \text{ litre atm}$, $\Delta H = 9.9 \text{ litre atm}$
5. -557 kJ/mol