

Elasticity

1. (B)

$$\Delta l = \frac{Fl}{\pi r^2 Y} \Rightarrow \frac{\Delta l_1}{\Delta l_2} = \left(\frac{F_1}{F_2}\right) \left(\frac{l_1}{l_2}\right) \left(\frac{r_2}{r_1}\right)^2$$

$$\Rightarrow \frac{l}{\Delta l_2} = \left(\frac{F}{2F}\right) \left(\frac{L}{2L}\right) \left(\frac{2r}{r}\right)^2$$

$$\Rightarrow \Delta l_2 = l$$

2. (C)

$$\text{Slope} = \frac{F}{\Delta l} = \frac{AY}{l} \Rightarrow \text{Slope} \propto A$$

Slope is least for wire A. So, wire A will be thinnest.

3. (A)

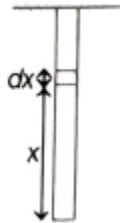
$$\Delta l = \frac{Fl}{AY},$$

$$\text{Slope} = \frac{\Delta l}{F} = \frac{(4-1) \times 10^{-4}}{80-20}$$

$$\Rightarrow \frac{l}{AY} = \frac{1}{20} \times 10^{-4}$$

$$\Rightarrow \frac{1}{10^{-6}Y} = \frac{1}{20} \times 10^{-4}$$

$$\Rightarrow Y = 2 \times 10^{11} \text{ N/m}^2$$



4. (B)

$$\Delta l = \frac{Fl}{AY}$$

$$\Rightarrow \frac{\Delta l_1}{\Delta l_2} = \left(\frac{F_1}{F_2}\right) \left(\frac{l_1}{l_2}\right) \left(\frac{r_2}{r_1}\right)^2 \left(\frac{Y_2}{Y_1}\right)$$

$$= \left(\frac{3mg}{2mg}\right) \left(a\right) \left(\frac{1}{b}\right)^2 \left(\frac{1}{c}\right) = \frac{3a}{2b^2c}$$

5. (C)

Let natural length be l .

$$F = kx$$

$$\Rightarrow T_1 = k(l_1 - l) \quad \dots\text{(i)}$$

$$\text{and } T_2 = k(l_2 - l) \quad \dots\text{(ii)}$$

Dividing Eq. (i) by Eq. (ii), we get

$$l = \frac{l_1 T_2 - l_2 T_1}{T_2 - T_1}$$

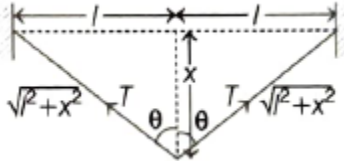
6. (A)
Breaking stress depends only on the material of wire.

7. (C)

$$T = \frac{2m_1m_2g}{m_1+m_2} = \frac{4mg}{3}$$

Breaking stress = $\frac{T}{A} \Rightarrow S = \frac{4mg}{\pi r^2} \Rightarrow r = \sqrt{\frac{4mg}{3\pi S}}$

8. (C)



$$\begin{aligned} \text{Strain} &= \frac{\Delta l}{l} = \frac{2\sqrt{l^2+x^2}-2l}{2l} = \left(1 + \frac{x^2}{l^2}\right)^{\frac{1}{2}} - 1 \\ &= 1 + \frac{x^2}{2l^2} - 1 \quad \{x \ll l\} \\ &= \frac{x^2}{2l^2} \end{aligned}$$

9. (D)
 $2 \cos \theta = w$

$$\Rightarrow T = \frac{w}{2 \cos \theta} = \frac{w\sqrt{l^2+x^2}}{2x}$$

$$\text{Stress} = \frac{T}{A} = \frac{w\sqrt{l^2+x^2}}{2xA} = \frac{wl}{2xA} \quad \because \{x \ll l\}$$

10. (A)

$$\Delta L = \frac{FL}{A\eta} = \frac{500 \times 0.04}{(4 \times 16 \times 10^{-4})(2 \times 10^6)} = 0.156 \times 10^{-2} \text{ m}$$

$$= 0.156 \text{ cm}$$

11. (D)
Bulk strain = $\frac{\Delta V}{V} = 3 \left(\frac{\Delta l}{l} \right) = 3 \left(\frac{2}{100} \right) = 0.06$

12. (B)

$$B = \frac{\Delta p}{\left(\frac{\Delta V}{V} \right)} \Rightarrow B = \frac{\rho gh}{\left(\frac{\Delta V}{V} \right)} = \frac{10^3 \times 10 \times 200}{\left(\frac{0.1}{100} \right)}$$

$$= 2 \times 10^9 \text{ N/m}^2$$

13. (B)

$$p = p_0 \rho^{\alpha V} \Rightarrow \frac{dp}{dV} = p_0 e^{\alpha V} (\alpha)$$

$$B = \frac{dp}{\left(\frac{dV}{V}\right)} = V \left(p_0 e^{\alpha V} \alpha \right) = \alpha p V$$

14. (D)

$$B = \frac{\Delta p}{\left(\frac{\Delta V}{V}\right)} \Rightarrow \frac{\Delta V}{V} = \frac{\Delta p}{B}$$

$$\Rightarrow \gamma \Delta T = \frac{p}{B} \Rightarrow \Delta T = \frac{p}{B\gamma}$$

15. (C)

Steel has the highest value of modulus of elasticity among the given materials.

16. (A)

$$\text{Longitudinal strain} = \frac{\text{Lateral strain}}{\sigma} = \frac{0.01 \times 10^{-3}}{0.4}$$

$$= 2.5 \times 10^{-5}$$

$$\text{Longitudinal stress} = \frac{F}{A} = \frac{100}{0.025} = 4 \times 10^3 \text{ N/m}^2$$

$$Y = \frac{4 \times 10^3}{2.5 \times 10^{-5}} = 1.6 \times 10^8 \text{ Nm}^{-2}$$

17. (A)

$$\frac{\Delta V}{V} = (1 - 2\sigma) \frac{\Delta l}{l} = (1 - 2(0.2)) (4 \times 10^{-3}) = 0.24 \times 10^{-2}$$

$$\frac{\Delta V}{V} \times 100 = (0.24 \times 10^{-2}) \times 100 = 0.24\%$$

18. (C)

$$\sigma_x = \sigma_y = \sigma_z = \frac{F}{A}$$

$$\text{In } x\text{-direction, Strain} = \frac{\sigma_x}{Y} - \sigma \left(\frac{\sigma_y}{Y} \right) - \sigma \left(\frac{\sigma_z}{Y} \right)$$

$$\Rightarrow \frac{\Delta l}{l} = \frac{F}{AY} (1 - 2\sigma)$$

$$\Rightarrow \Delta l = \frac{F}{AY} (1 - 2\sigma)$$

19. (A)

Energy per unit volume

$$= \frac{1}{2} Y (\text{Strain})^2 = \frac{1}{2} \times 2 \times 10^{10} \times \left(\frac{0.06}{100} \right)^2$$

$$= 3600 \text{ Jm}^{-3}$$

20. (D)

$$\sigma = \frac{F}{A} = \frac{F}{\pi r^2} \Rightarrow \sigma \propto \frac{1}{r^2} \Rightarrow \frac{\sigma_1}{\sigma_2} = \left(\frac{r_2}{r_1} \right)^2$$

$$U = \frac{(\text{Stress})^2}{2Y} \Rightarrow U \propto \sigma^2$$

$$\Rightarrow \frac{U_1}{U_2} = \left(\frac{\sigma_1}{\sigma_2} \right)^2 = \left(\frac{r_2}{r_1} \right)^4$$

$$= \left(\frac{2r}{r} \right)^4 = 16:1$$

21. (B)

$$k_{\text{eq}} = k_1 + k_2 \Rightarrow \frac{(2A)Y_{\text{eq}}}{L} = \frac{AY_1}{L} + \frac{AY_2}{L}$$

$$\Rightarrow Y_{\text{eq}} = \frac{Y_1 + Y_2}{2}$$

22. (D)

For no change in the lengths of individual rods, the compressive forces in both rods due to thermal expansion should be equal. So,

$$A_1 Y_1 \alpha_1 \Delta T = A_2 Y_2 \alpha_2 \Delta T$$

$$\Rightarrow \frac{A_1}{A_2} = \frac{\alpha_2 Y_2}{\alpha_1 Y_1}$$

23. (B)

$$E = \frac{\text{Stress}}{\text{Strain}} \Rightarrow E = \frac{\frac{F}{A}}{\left(\frac{2\pi R - 2\pi r}{2\pi r} \right)}$$

$$\Rightarrow F = AE \left(\frac{R-r}{r} \right)$$

Surface Tension

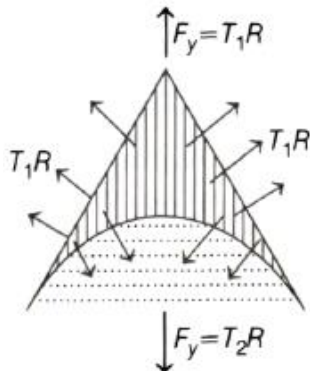
24. (D)

For equilibrium of wire ab ,

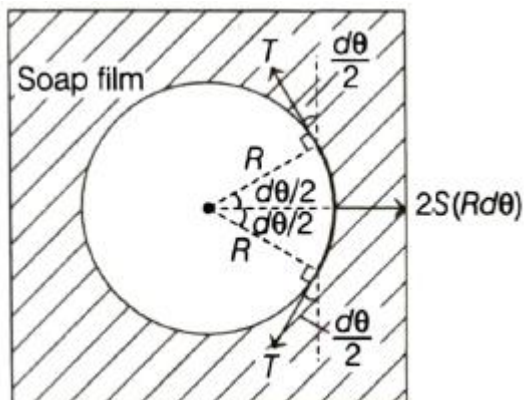
$$2Tl = mg$$

$$\Rightarrow m = \frac{2Tl}{g} = \frac{2 \times 25 \times 10^{-3} \times 0.1}{10} = 0.5 \text{ g}$$

25. (B)
 $F_y = T \times \text{Projected length}$
 Net force $= T_1 R - T_2 R$
 $= (T_1 - T_2) R$ in +y-direction



26. (D)
 Lets take an element of angular width $d\theta$ on the thread.



Force on the element due to surface tension
 $= 2S(Rd\theta)$

For equilibrium of element,

$$2T \sin\left(\frac{d\theta}{2}\right) = 2SRd\theta$$

$$\Rightarrow 2T\left(\frac{d\theta}{2}\right) = 2SRd\theta \Rightarrow T = 2SR$$

27. (B)
 Let radius of single large drop be R .
 For volume conservation, $2\left(\frac{4}{3}\pi r^3\right) = \frac{4}{3}\pi R^3$
 $\Rightarrow R = 2^{1/3}r$
 $U_1 = T(4\pi r^2) \times 2$
 $U_2 = T(4\pi R^2)$

$$\frac{U_2}{U_1} = \frac{T(8\pi r^2)}{T(4\pi r^2)} = \frac{2r^2}{(2^{1/3}r)^2} = 2^{1/3} : 1$$

28. (B)

$$U_1 = S \left[2 \times 4\pi \left(\frac{d}{2} \right)^2 \right], \quad U_2 = S \left[2 \times 4\pi \left(\frac{2d}{2} \right)^2 \right]$$

$$W = \Delta U = U_2 - U_1 = 6\pi d^2 S$$

29. (D)

$$W = T(4\pi r^2 \times 2)$$

$$= T \left[4\pi \left\{ \left(\frac{3V}{4\pi} \right)^{1/3} \right\}^2 \times 2 \right] \quad \left\{ \because V = \frac{4}{3}\pi r^3 \Rightarrow r = \left(\frac{3V}{4\pi} \right)^{1/3} \right\}$$

$$\Rightarrow W \propto V^{2/3}$$

$$\Rightarrow \frac{W_1}{W_2} = \left(\frac{V_1}{V_2} \right)^{2/3} \Rightarrow \frac{W}{W_2} = \left(\frac{V}{2V} \right)^{2/3}$$

$$\Rightarrow W_2 = 2^{2/3} W = \sqrt[3]{4} W$$

30. (B)

$$\text{From volume conservation, } \frac{4}{3}\pi R^3 = n \left(\frac{4}{3}\pi r^3 \right)$$

$$\Rightarrow r = \frac{R}{n^{1/3}}$$

$$U_1 = T(4\pi R^2)$$

$$U_2 = nT(4\pi r^2) = n4\pi T \left(\frac{R}{n^{1/3}} \right)^2 = n^{1/3} T(4\pi R^2)$$

$$W = \Delta U = U_2 - U_1 = (n^{1/3} - 1) T(4\pi R^2)$$

31. (A)

$$U = T(8\pi r^2)$$

$$P = \frac{dU}{dt} = T(8\pi) \left(2r \frac{dr}{dt} \right)$$

$$\Rightarrow P \propto r \quad \because \left\{ \frac{dr}{dt} \text{ is constants} \right\}$$

So, P versus r graph will be straight line passing through origin.

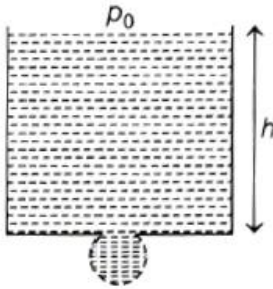
32. (C)
Air bubble inside water has only one free surface.

So, excess pressure will be $\frac{2T}{r}$.

$$p = (p_0 + gh) + \frac{2T}{r}$$

33. (A)
Pressure difference on two sides of a curved surface is inversely proportional to the radius of curvature.

34. (D)



$$p_0 + \rho gh - \frac{2T}{r} = p_0$$

$$\Rightarrow h = \frac{2T}{\rho gr} = \frac{2 \times 70}{1 \times 1000 \times 0.005} = 28.0 \text{ cm}$$

35. (D)
 $h = \frac{2T \cos \theta}{\rho g_{\text{eff}} R}$
For a freely falling elevator, $g_{\text{eff}} = 0 \Rightarrow h \rightarrow \infty$
So, capillary will be completely filled with water.

36. (B)
 $H = \frac{2T \cos \theta}{\rho g R} \Rightarrow H \propto \frac{1}{R}$
So, when radius is double, H will be halved.

$$M' = \rho \left[\pi (2R)^2 \left(\frac{H}{2} \right) \right] \text{ and } M = \rho (\pi R^2 H)$$

$$\frac{M'}{M} = 2 \Rightarrow M' = 2M$$

37. (D)
 $T(2\pi r) \cos \theta = w$

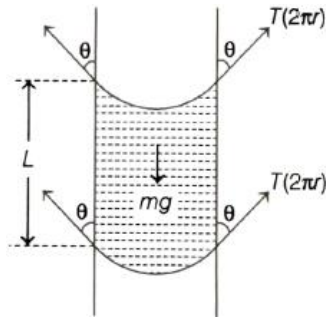
$$\Rightarrow \text{Circumference} = 2\pi r = \frac{w}{T \cos \theta}$$

$$= \frac{75 \times 10^{-4}}{6 \times 10^{-2} \cos 0^\circ} = 12.5 \times 10^{-2} \text{ m}$$

38. (A)

For equilibrium of water column,

$$T(2\pi r)\cos\theta + T(2\pi r)\cos\theta = mg$$

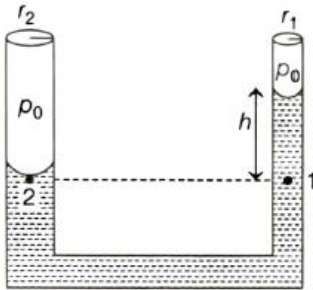


$$\Rightarrow T(4\pi r)\cos\theta = (\rho\pi r^2 L)g \Rightarrow O = \frac{4T}{\rho g r}$$

39. (A)

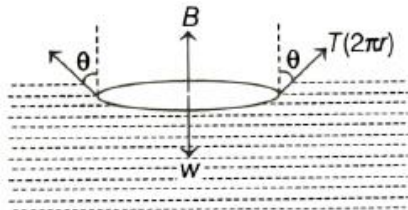
$$p_1 = p_2$$

$$\Rightarrow p_0 - \frac{2T}{r_2} = p_0 - \frac{2T}{r_1} + \rho g h \Rightarrow T = \frac{\rho g h r_1 r_2}{2(r_2 - r_1)}$$



40. (C)

$$\Sigma F_y = 0 \Rightarrow B + T(2\pi r)\cos\theta = w_{\text{disc}}$$



$$\Rightarrow w_{\text{disc}} = w + 2\pi r T \cos\theta$$

Viscosity

41. (A)

$$v_T = \frac{2(\sigma)r^2g}{9\eta}$$

$$\Rightarrow v_T = \frac{2}{9} \times \frac{10^3 \times (0.3 \times 10^{-3})^2 \times 9.8}{1.8 \times 10^{-5}} = 10.9 \text{ m/s}$$

42. (B)

$$m = \sigma \left(\frac{4}{3} \pi r^3 \right)$$

$$\Rightarrow \sigma \propto \frac{1}{r^3} \Rightarrow \frac{\sigma_1}{\sigma_2} = \frac{r_2^3}{r_1^3}$$

$$\Rightarrow \sigma_2 = 8\sigma_1$$

$$v_T = \frac{2}{9} \frac{\sigma r^2 g}{\eta}$$

$$\Rightarrow \frac{v_1}{v_2} = \left(\frac{\sigma_1}{\sigma_2} \right) \left(\frac{r_1}{r_2} \right)^2$$

$$\Rightarrow \frac{v}{v_2} = \left(\frac{\sigma_1}{8\sigma_1} \right) \left(\frac{r_1}{r_2} \right)^2$$

$$\Rightarrow v_2 = 2v$$

43. (C)

$$mg - B - 6\pi\eta r v = ma$$

So, a versus v graph will straight line with negative slope.

Hence, option (C) is incorrect.

44. (B)

From volume conservation,

$$2 \left(\frac{4}{3} \pi r^3 \right) = \frac{4}{3} \pi R^3$$

$$\Rightarrow R = (2)^{1/3} r$$

$$v_T \propto r^2 \Rightarrow \frac{v_1}{v_2} = \left(\frac{r_1}{r_2} \right)^2 \Rightarrow \frac{v}{v_2} = \left(\frac{r}{2^{1/3} r} \right)^2$$

$$\Rightarrow v_2 = (4^{1/3})v$$

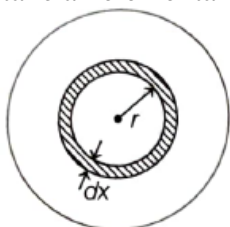
45. (D)

$$2\eta A \frac{dv}{dx} = mg \Rightarrow 2\eta A \frac{dv}{dx} = (\rho A d) g$$

$$\Rightarrow \frac{dv}{dx} = \frac{\rho d g}{2\eta}$$

46. (C)

Lets take an elemental ring of radius r and thickness dr on the disc.



$$F = \eta A \frac{dv}{dx} \Rightarrow dF = \eta(2\pi r dr) \left(\frac{\omega r - 0}{t} \right)$$

$$\int d\tau = \int_0^R \eta(2\pi r dr) \left(\frac{\omega r}{t} \right) r$$

$$\Rightarrow \tau \propto R^4$$

47. (C)

$$R_e = \frac{\rho v d}{\eta} = \frac{1 \times 6 \times 2}{0.01} = 1200$$

48. (B)

$$v_T = \frac{2(\sigma - \rho)r^2 g}{9\eta}$$

$$\Rightarrow 8 = \frac{2(10.5 - 1.5)(0.2) \times 980}{9\eta}$$

$$\Rightarrow \eta = 9.8 \text{ poise}$$

Numerical Value Answer

Elasticity

49. (200)

$$F = \sigma A = \sigma(2\pi r t)$$

$$= 3.45 \times 10^8 \left(2 \times 3.14 \times 0.73 \times 10^{-2} \times 1.24 \times 10^{-2} \right) = 200 \text{ kN}$$

50. (8)

$$k = \frac{(\pi r^2)Y}{L} \Rightarrow \frac{k_1}{k_2} = \left(\frac{r_1}{r_2} \right)^2 = \frac{1}{4}$$

$$\Delta l_1 + \Delta l_2 = 10 \text{ mm} \quad \dots(\text{i})$$

$$k_1 \Delta l_1 = k_2 \Delta l_2 \Rightarrow \frac{\Delta l_1}{\Delta l_2} = \frac{k_2}{k_1} = 4 \quad \dots(\text{ii})$$

Solving Eqs. (i) and (ii), we get

$$\Delta l_1 = 8 \text{ mm}$$

51. (1025)

Consider 1 m^3 of water at the surface. Let us calculate change in volume ΔV of this water when it is at a pressure of 501 atm.

$$\Delta V = \frac{(\Delta p)V}{B} = \left(\frac{501 - 1 \times 10^5 \times 1}{2 \times 10^9} \right) = 0.025 \text{ m}^3$$

$$\text{New density} = \frac{m}{V - \Delta V} = \frac{1000}{1 - 0.025} = 1025 \text{ kg m}^{-3}$$

52. (3)

$$\sigma = \frac{T}{A} = \frac{m(g+a)}{A}$$

$$\begin{aligned} \text{Strain} &= \frac{\sigma}{Y} = \frac{m(g+a)}{AY} \\ &= \frac{10(10+2)}{2 \times 10^{-4} \times 2 \times 10^{11}} = 3 \times 10^{-6} \end{aligned}$$

53. (4)

$$F = \left(\frac{AY}{l} \right) \Delta l \Rightarrow \text{Force constant} = \frac{AY}{l}$$

$$\omega = \sqrt{\frac{k}{m}} = \sqrt{\frac{AY}{ml}} = \sqrt{\frac{4.9 \times 10^{-7} Y}{0.1 \times 1}} = 140$$

$$\Rightarrow Y = 4 \times 10^9 \text{ Nm}^{-2}$$

Surface Tension

54. (4)

$$B = \frac{\Delta p}{\left(\frac{\Delta V}{V} \right)} \Rightarrow \frac{\Delta p}{V} = \frac{\Delta p}{B} \Rightarrow \frac{3\Delta R}{R} = \frac{2T}{BR}$$

$$\Rightarrow \Delta R = \frac{2T}{3B} = \frac{2 \times 0.075}{3 \times 1.25 \times 10^8} = 4 \times 10^{-10} \text{ m} = 4 \text{ \AA}$$

55. (450)

$$h = \frac{2T \cos \theta}{\rho g R}$$

$$\Rightarrow 3 = \frac{2T \cos 0^\circ}{1.5 \times 1000 \times 0.25 \times 10^{-1}}$$

$$\Rightarrow T = 56.25 \text{ dyne / cm}$$

$$\Delta p = \frac{4T}{r} = \frac{4 \times 56.25}{0.5} = 450 \text{ dyne/cm}^2$$

56. (3)

For an isothermal situation,

$$p_A V_A + p_B V_B = p_c V_c$$

$$\Rightarrow \left(p_0 + \frac{5T}{a} \right) \left(\frac{4}{3} \pi a^3 \right) + \left(p_0 + \frac{4T}{b} \right) \left(\frac{4}{3} \pi b^3 \right)$$

$$= \left(p_0 + \frac{4T}{c} \right) \left(\frac{4}{3} \pi c^3 \right)$$

$$\Rightarrow p_0 \left(\frac{4}{3} \pi a^3 + \frac{4}{3} \pi b^3 - \frac{4}{3} \pi c^3 \right) + \frac{4T}{3} (4\pi a^2 + 4\pi b^2 - 4\pi c^2) = 0$$

$$\Rightarrow p_0 V + \left(\frac{4T}{3} \right) S = 0 \Rightarrow 3p_0 V + 4TS = 0$$

So, $\lambda = 3$

57. (2.4)

$$p = p_0 + \rho gh + \frac{2T}{R}$$
$$= 10^5 + 10^3 \times 10 \times 6 + \frac{2 \times 0.07}{3.5 \times 10^{-6}} = 2 \times 10^5 \text{ Pa}$$

$$\rho = \frac{pM}{RT} \Rightarrow \frac{\rho_1}{\rho_2} = \frac{p_1}{p_2}$$

$$\Rightarrow \frac{1.2}{\rho_2} = \frac{10^5}{2 \times 10^5}$$

$$\Rightarrow \rho_2 = 2.4 \text{ kg/m}^3$$

58. (9)

$$\text{Initial pressure inside bubble} = p_0 + \frac{4T}{r}$$

$$\text{Final pressure inside bubble} = p_{\text{new}} + \frac{4T}{(r/2)}$$

For isothermal condition,

$$p_1 V_1 = p_2 V_2$$

$$\Rightarrow \left(p_0 + \frac{4T}{r} \right) \left(\frac{4}{3} \pi r^3 \right) = \left(p_{\text{new}} + \frac{8T}{r} \right) \frac{4}{3} \pi \left(\frac{r}{2} \right)^3$$

$$\Rightarrow p_{\text{new}} = 8p_0 + \frac{24T}{r} = 8 \times 10^5 + \frac{24 \times 0.08}{1.92 \times 10^{-5}}$$
$$= 9 \times 10^5 \text{ N/m}^2$$

Viscosity

59. (20.4)

$$v_T = \frac{2(\sigma - \rho)r^2 g}{9\eta} = \sqrt{2gh}$$

$$\Rightarrow \frac{2(10^4 - 10^3)(1 \times 10^{-4})^2 (9.8)}{9 \times 9.8 \times 10^{-6}} = \sqrt{2 \times 9.8 h}$$

$$\Rightarrow h = 20.4 \text{ m}$$

60. (9)

F_1 = Viscous force on upper surface

$$= \eta A \frac{dv}{dx} = \eta A \left(\frac{v-0}{d/2} \right) = 2\eta \frac{Av}{d}$$

$$F_2 = \text{viscous force on lower surface} = \frac{2\eta Av}{d}$$

$$F_{\text{ext}} = F_1 + F_2 = \frac{4\eta Av}{d}$$

$$= \frac{4(150 \times 10^{-1})(0.1)^2(3 \times 10^{-2})}{2 \times 10^{-3}} = 9 \text{ N}$$

61. (50)

In fluid frame, ball is moving with constant velocity and resultant of all forces acting on it is zero.

$$v_T = \frac{2(\rho - \sigma)r^2g}{9\eta}$$

$$= \frac{2(1000 - 100)(0.05)^2(10)}{9 \cdot 0.1}$$

$$= 50 \text{ m/s}$$

62. (5)

Rate of production of heat = $P = Fv_T = (6\pi\eta rV_T)v_T$

$$P \propto rv_T^2$$

$$P \propto r^5 \because \{v_T \propto r^2\}$$

1. (D)

$$(d) \quad Y_c \times (\Delta L_c / L_c) = Y_s \times (\Delta L_s / L_s)$$

$$\Rightarrow 1 \times 10^{11} \times \left(\frac{1 \times 10^{-3}}{1} \right) = 2 \times 10^{11} \times \left(\frac{\Delta L_s}{0.5} \right)$$

$$\therefore \Delta L_s = \frac{0.5 \times 10^{-3}}{2} = 0.25 \text{ mm}$$

Therefore, total extension of the composite wire

$$= \Delta L_c + \Delta L_s = 1 \text{ mm} + 0.25 \text{ mm} = 1.25 \text{ mm}$$

2. (C)

(c) According to questions,

$$\frac{l_s}{l_b} = a, \quad \frac{r_s}{r_b} = b, \quad \frac{y_s}{y_b} = c, \quad \frac{\Delta l_s}{\Delta l_b} = ?$$

$$\text{As, } y = \frac{F l}{A \Delta l} \Rightarrow \Delta l = \frac{F l}{A y}$$

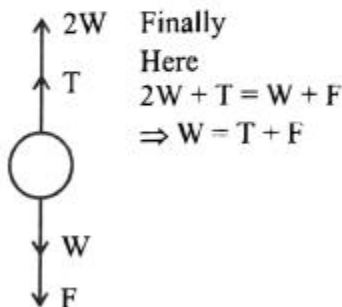
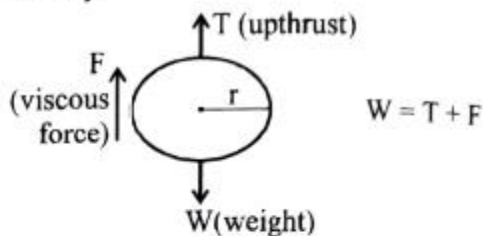
$$\Delta l_s = \frac{3 M g l_s}{\pi r_s^2 \cdot y_s} \quad [\because F_s = (M + 2M)g]$$

$$\Delta l_b = \frac{2 M g l_b}{\pi r_b^2 \cdot y_b} \quad [\because F_b = 2Mg]$$

$$\therefore \frac{\Delta l_s}{\Delta l_b} = \frac{\frac{3 M g l_s}{\pi r_s^2 \cdot y_s}}{\frac{2 M g l_b}{\pi r_b^2 \cdot y_b}} = \frac{3a}{2b^2 c}$$

3. (C)

(c) Initially



So in both case $W = T + F$

So, in both case state of body will be same.

4. (B)

(b) $F = \eta A \frac{dv}{dx}$

$$\frac{F}{A} = \eta \frac{dv}{dx} = 10^{-2} \times \frac{5}{5} = 10^{-2} \text{ N/m}^2$$

5. (B)

(b) According to Toricelli's theorem,
Velocity of efflux,

$$V_{\text{eff}} = \sqrt{2gh} = \sqrt{2 \times 9.8 \times 5} \cong 9.8 \text{ ms}^{-1}$$

6. (C)

(c) Poisson's ratio, $\sigma = \frac{\text{lateral strain } (\beta)}{\text{longitudinal strain } (\alpha)}$

For material like copper, $\sigma = 0.33$

And, $Y = 3k(1 - 2\sigma)$ Also, $\frac{9}{Y} = \frac{1}{k} + \frac{3}{\eta}$

$Y = 2\eta(1 + \sigma)$ Hence, $\eta < Y < k$

7. (A)

(a) When the bubble gets detached,

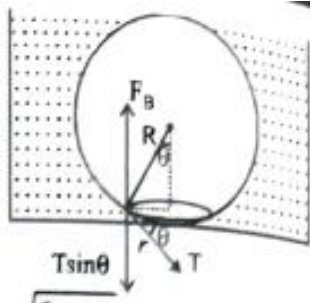
Buoyant force = force due to surface tension from diagram

$$\sin \theta = \frac{r}{R}$$

$$\rho_{\omega} V g = (T \sin \theta) \times (2\pi r)$$

$$\Rightarrow \rho_{\omega} \times \frac{4}{3} \pi R^3 g = T \cdot \frac{r}{R} \times 2\pi r$$

$$\Rightarrow \rho_{\omega} \frac{4}{3} R^3 g = \frac{2T}{R} r^2 \Rightarrow r = R^2 \sqrt{\frac{2\rho_{\omega} g}{3T}}$$



8. (A)
Inside a drop or an air bubble, towards concave side

$$P = P_0 + \frac{2T}{R} \Rightarrow \Delta P = \frac{2T}{R}$$

Here, the figure shows that the water between the plates formed a curved surface, similar to that formed by air bubble inside the water. So, pressure in water between the plates is lowered by $\frac{2T}{R}$.

9. (C)
When a point mass is falling vertically in a viscous medium, the medium or viscous fluid exerts drag force on the body to oppose its motion and at one stage body falling with constant terminal velocity.

10. (A)
Young's modulus $Y = \frac{F}{A} \bigg/ \frac{\Delta \ell}{\ell}$
 $Y = \frac{F \ell}{\pi r^2 \Delta \ell}$
Given, radius $r = 5$ mm, force $F = 50\pi k$ N,

$$\frac{\ell}{\Delta \ell} = 0.01 \text{ mm}$$

$$\therefore Y = \frac{F}{\pi r^2} \frac{\ell}{\Delta \ell} = 2 \times 10^{14} \text{ N/m}^2$$

11. (D)
Stress = $\frac{\text{Normal force}}{\text{Area}} = \frac{N}{A} = \frac{N}{(2\pi a)b}$

$$V = \pi a^2 b$$

$$\Delta V = 2\pi a b \Delta a$$

$$\text{Stress} = B \times \text{strain}$$

$$\frac{N}{(2\pi a)b} = B \frac{2\pi a \Delta a \times b}{\pi a^2 b} \left[\because \text{Strain} = \frac{\Delta V}{V} \right]$$

$$\Rightarrow N = B \frac{(2\pi a)^2 \Delta a b^2}{\pi a^2 b}$$

For needed to push the cork.

$$f = \mu N = \frac{\mu \times B \times 4\pi^2 a^2 b^2 \Delta a}{\pi a^2 b} = (4\pi\mu B b) \Delta a$$

12. (C)

(c) Bulk modulus, $K = \frac{\text{volumetric stress}}{\text{volumetric strain}}$

$$K = \frac{mg}{a \left(\frac{dV}{V} \right)} \quad \left[\because \text{Stress} = \frac{F}{A} = \frac{mg}{a} \right]$$

$$\Rightarrow \frac{dV}{V} = \frac{mg}{Ka} \quad \dots(i)$$

volume of sphere, $V = \frac{4}{3}\pi r^3$

Fractional change in volume $\frac{dV}{V} = \frac{3dr}{r} \quad \dots(ii)$

Using eq. (i) & (ii) $\frac{3dr}{r} = \frac{mg}{Ka}$

$$\therefore \frac{dr}{r} = \frac{mg}{3Ka} \quad (\text{fractional decrement in radius})$$

13. (B)

(b) As we know that

$$\frac{2T \cos \theta}{r\rho g} = R h \quad \text{or} \quad \frac{T_{\text{Hg}}}{T_{\text{Water}}} = 7.5$$

$$\frac{\rho_{\text{Hg}}}{\rho_{\text{W}}} = 13.6 \quad \& \quad \frac{\cos \theta_{\text{Hg}}}{\cos \theta_{\text{W}}} = \frac{\cos 135^\circ}{\cos 0^\circ} = \frac{1}{\sqrt{2}}$$

$$\frac{R_{\text{Hg}}}{R_{\text{Water}}} = \left(\frac{T_{\text{Hg}}}{T_{\text{W}}} \right) \left(\frac{\rho_{\text{W}}}{\rho_{\text{Hg}}} \right) \left(\frac{\cos \theta_{\text{Hg}}}{\cos \theta_{\text{W}}} \right)$$

$$= 7.5 \times \frac{1}{13.6} \times \frac{1}{\sqrt{2}} = 0.4 = \frac{2}{5}$$

14. (D)

(d) We have, $h = \frac{2T \cos \theta}{r\rho g}$

Mass of the water in the capillary

$$m = \rho V = \rho \times \pi r^2 h = \rho \times \pi r^2 \times \frac{2T \cos \theta}{r\rho g} \Rightarrow m \propto r$$

$$\therefore \frac{m_1}{m_2} = \frac{r}{2r} \quad \text{or} \quad m_2 = 2m_1 = 2m.$$

15. (A)

$$(a) 27 \times \frac{4}{3} \pi r^3 = \frac{4}{3} \pi R^3 \text{ or } r = \frac{R}{3}.$$

Terminal velocity, $v \propto r^2$

$$\therefore \frac{v_1}{v_2} = \frac{r_1^2}{r_2^2} \text{ or } v_2 = \left(\frac{r_2}{r_1}\right)^2 v_1 = \left(\frac{R/3}{R}\right)^2 v_1 = \frac{1}{9}$$

$$\text{or } \frac{v_1}{v_2} = 9.$$

16. (C)

$$(c) \Delta_{\text{temp}} = \Delta_{\text{force}}$$

$$\text{or } L\alpha(\Delta T) = \frac{FL}{AY} \quad \therefore \alpha = \frac{FL}{AYT} = \frac{F}{\pi r^2 Y T}$$

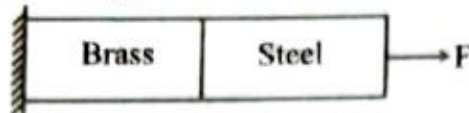
Coefficient of volume expansion

$$r = 3\alpha = \frac{3F}{\pi r^2 Y T}$$

17. (None)

$$\text{(None) Young modulus, } Y = \frac{\text{Stress}}{\left(\frac{\Delta l}{L}\right)}$$

Let σ be the stress.



$$\text{Total elongation } \Delta l_{\text{net}} = \frac{\sigma L_1}{Y_1} + \frac{\sigma L_2}{Y_2}$$

$$\Delta l_{\text{net}} = \sigma \left[\frac{1}{Y_1} + \frac{1}{Y_2} \right] \quad [\because L_1 = L_2 = 1\text{m}]$$

$$\begin{aligned} \sigma &= \Delta l \left(\frac{Y_1 Y_2}{Y_1 + Y_2} \right) = 0.2 \times 10^{-3} \times \left(\frac{120 \times 60}{180} \right) \times 10^9 \\ &= 8 \times 10^6 \frac{\text{N}}{\text{m}^2} \end{aligned}$$

18. (B)

$$(b) \text{ Stress} = \frac{F}{A} = \frac{400 \times 4}{\pi d^2} = 379 \times 10^6 \text{ N/m}^2$$

$$\Rightarrow d^2 = \frac{400 \times 4}{379 \times 10^6 \pi} \Rightarrow d = 1.15 \text{ mm}$$

19. (C)

$$(c) \Delta_1 = \Delta_2$$

$$\text{or } \frac{Fl_1}{\pi r_1^2 y_1} = \frac{Fl_2}{\pi r_2^2 y_2} \text{ or } \frac{2}{R^2 \times 7} = \frac{1.5}{2^2 \times 4}$$

$$\therefore R = 1.75 \text{ mm}$$

20. (A)

(a) When a catapult is stretched up to length l , then the

$$\text{stored energy in it} = \Delta k. E \Rightarrow \frac{1}{2} \cdot \left(\frac{YA}{L} \right) (\Delta l)^2 = \frac{1}{2} mv^2$$

$$\Rightarrow y = \frac{mv^2 L}{A(\Delta l)^2}$$

$$m = 0.02 \text{ kg}, v = 20 \text{ ms}^{-1}, L = 0.42 \text{ m}, A = (\pi d^2)/4$$

$$d = 6 \times 10^{-3} \text{ m}, \Delta l = 0.2 \text{ m}$$

$$y = \frac{0.02 \times 400 \times 0.42 \times 4}{\pi \times 36 \times 10^{-6} \times 0.04} = 2.97 \times 10^6 \text{ N/m}^2$$

So, order is 10^6 .

21. (A)

(a) If force F acts along the length L of the wire of cross-section A , then energy stored in unit volume of wire is given by

$$\text{Energy density} = \frac{1}{2} \text{ stress} \times \text{strain}$$

$$= \frac{1}{2} \times \frac{F}{A} \times \frac{F}{AY} \left(\because \text{stress} = \frac{F}{A} \text{ and strain} = \frac{F}{AY} \right)$$

$$= \frac{1}{2} \frac{F^2}{A^2 Y} = \frac{1}{2} \frac{F^2 \times 16}{(\pi d^2)^2 Y} = \frac{1}{2} \frac{F^2 \times 16}{\pi d^4 Y}$$

If u_1 and u_2 are the densities of two wires, then

$$\frac{u_1}{u_2} = \left(\frac{d_2}{d_1} \right)^4 \Rightarrow \frac{d_1}{d_2} = (4)^{1/4} \Rightarrow \frac{d_1}{d_2} = \sqrt{2} : 1$$

22. (C)

(c) According to question, pressure inside, 1st soap bubble,

$$\Delta P_1 = P_1 - P_0 = 0.01 = \frac{4T}{R_1} \quad \dots(i)$$

$$\text{And } \Delta P_2 = P_2 - P_0 = 0.02 = \frac{4T}{R_2} \quad \dots(ii)$$

Dividing, equation (ii) by (i),

$$\frac{1}{2} = \frac{R_2}{R_1} \Rightarrow R_1 = 2R_2$$

$$\text{Volume } V = \frac{4}{3}\pi R^3 \Rightarrow \frac{V_1}{V_2} = \frac{R_1^3}{R_2^3} = \frac{8R_2^3}{R_2^3} = \frac{8}{1}$$

23. (B)

(b) Given, Weight of uniform heavy rod. $W = 10 \text{ kg ms}^{-2}$

Length of rod, $L = 20 \text{ cm} = 0.2 \text{ m}$

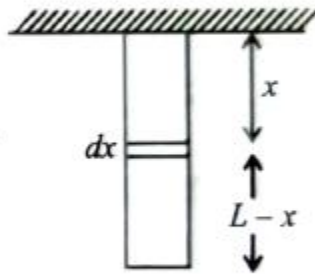
Consider an element dx at distance x from top.

Force acting on part below dx

$$= \frac{(L-x)W}{L}$$

Elongation for small element dx , dl

$$= \left(\frac{L-x}{L}\right) \frac{Wdx}{AY}$$



$$\int_0^L dl = \int \left(\frac{L-x}{L}\right) \frac{w dx}{AY} \Rightarrow \Delta \ell = \frac{WL}{2AY} = 5 \times 10^{-9} \text{ m}$$

24. (B)

(b) Force exerted on each column $F = \frac{mg}{4}$

$$\therefore y = \frac{F}{A} / \frac{\Delta \ell}{\ell}$$

$$\therefore \text{Strain} \left(\frac{\Delta \ell}{\ell}\right) = \frac{mg}{4AY}$$

$$= \frac{50 \times 10^3 \times 9.8}{4 \times [\pi \times 1^2 - \pi(.5)^2]} = 2.6 \times 10^{-7} \quad [\because A = \pi r^2]$$

25. (C)

(c) Here, $m_1 = 3\text{ kg}$, $m_2 = 5\text{ kg}$

Tension in the metal wire.

$$T = \frac{2m_1m_2g}{m_1 + m_2} = \frac{2 \times 3 \times 5 \times 10}{8} = \frac{75}{2}$$

$$\text{Stress} = \frac{T}{A} = \frac{T}{\pi r^2}$$

$$\Rightarrow \frac{24}{\pi} \times 10^2 = \frac{75}{2 \times \pi r^2} \Rightarrow r^2 = \frac{75}{2 \times 24 \times 100} = \frac{3}{8 \times 24}$$

$$\Rightarrow r = 0.125\text{ m} = 12.5\text{ cm}$$

26. (A)

(a) Bulk modulus (K) is given by $K = \frac{P}{\left(-\frac{\Delta V}{V}\right)}$

$$\text{Density, } \rho = \frac{m}{V}$$

$$\text{So, } \frac{\Delta \rho}{\rho} = \frac{+\Delta V}{V} \therefore K = \frac{P}{\left(\frac{\Delta \rho}{\rho}\right)} \Rightarrow \frac{\Delta \rho}{\rho} = \frac{P}{K} \Rightarrow \Delta \rho = \frac{\rho P}{K}$$

27. (D)

(d) We know that

$$Y = 3K(1 - 2\sigma)$$

Here,

$\sigma = \text{Poisson's ratio}$

$$\sigma = \frac{1}{2} \left(1 - \frac{Y}{3K}\right)$$

Also,

$$Y = 2\eta(1 + \sigma)$$

$$\sigma = \frac{Y}{2\eta} - 1$$

From equation (i) and equation (ii),

$$\frac{1}{2} \left(1 - \frac{Y}{3K}\right) = \frac{Y}{2\eta} - 1$$

$$\Rightarrow 1 - \frac{Y}{3K} = \frac{Y}{\eta} - 2 \Rightarrow \frac{Y}{3K} = 3 - \frac{Y}{\eta} \Rightarrow \frac{Y}{3K} = \frac{3\eta - Y}{\eta}$$

$$\Rightarrow \frac{\eta Y}{3K} = 3\eta - Y \Rightarrow K = \frac{\eta Y}{9\eta - 3Y}$$

28. (B)

(b) Pressure at same horizontal level is equal

$$\text{So, } P_1 = P_2$$

$$P_3 = P_{atm} - \frac{2T}{r_1}$$

$$\& P_4 = P_{atm} - \frac{2T}{r_2}$$

$$P_2 = P_4 + \rho g h_2 = P_{atm} - \frac{2T}{r_2} + \rho g h_2$$

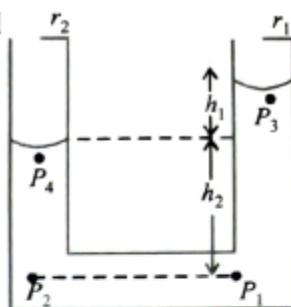
$$\& P_1 = P_3 + \rho g (h_1 + h_2) = P_{atm} - \frac{2T}{r_1} + \rho g (h_1 + h_2)$$

$$\therefore P_{atm} - \frac{2T}{r_1} + \rho g (h_1 + h_2) = P_{atm} - \frac{2T}{r_2} + \rho g h_2$$

$$\therefore \rho g h_1 = 2T \left[\frac{1}{r_1} - \frac{1}{r_2} \right]$$

$$= 2 \times 7.3 \times 10^{-2} \left[\frac{1}{2.5 \times 10^{-3}} - \frac{1}{4 \times 10^{-3}} \right]$$

$$\Rightarrow h_1 = 2.19 \times 10^{-3} \text{ m} = 2.19 \text{ mm}$$



29. (A)

(a) As volume remain same i.e volume of two smaller drops will be equal to volume of one big drop.

$$2 \times \frac{4}{3} \pi r^3 = \frac{4}{3} \pi R^3 \Rightarrow 2r^3 = R^3$$

$$\Rightarrow 2 = \left(\frac{R}{r} \right)^3 \Rightarrow \frac{R}{r} = 2^{\frac{1}{3}}$$

$$\frac{U_i}{U_f} = \frac{T \times 2 \times (4\pi r^2)}{T \times 4\pi R^2} = \frac{2r^2}{2^{\frac{2}{3}} R^2} = 2^{\frac{1}{3}}$$

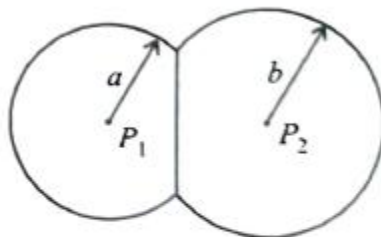
30. (A)

(a) Let R be the radius of curvature of common surface

$$P_1 = P_0 + \frac{4T}{a} \text{ and}$$

$$P_2 = P_0 + \frac{4T}{b}$$

$$\text{And } P_1 - P_2 = \frac{4T}{R}$$



$$\left(P_0 + \frac{4T}{a} \right) - \left(P_0 + \frac{4T}{b} \right) = \frac{4T}{R}$$

$$\Rightarrow \frac{1}{a} - \frac{1}{b} = \frac{1}{R} \quad \therefore R = \frac{ab}{(b-a)}$$

31. (C)

(c) As volume remains unchanged

$$n \times \frac{4}{3} \pi r^3 = \frac{4}{3} \pi R^3 \Rightarrow nr^3 = R^3$$

Work done = $T \times$ Increment in surface area

$$W = T[4\pi nr^2 - 4\pi R^2] \dots(i)$$

By conservation of energy

Loss in thermal energy = work done against surface tension

$$JQ = W$$

Where J = mechanical equivalent of heat

$$Q = \frac{W}{J} = \frac{4\pi T(nr^2 - R^2)}{J} \quad [\text{Using (i)}]$$

Heat energy per unit volume

$$\begin{aligned} Q &= \frac{4\pi T}{Jn \cdot \frac{4}{3} \pi r^3} [nr^2 - R^2] = \frac{4\pi T}{J \times \frac{4}{3} \pi} \left[\frac{1}{r} - \frac{R^2}{nR^3} \right] \\ &= \frac{3T}{J} \left[\frac{1}{r} - R^2 \right] = \frac{3T}{J} \left[\frac{1}{r} - \frac{1}{R} \right] \end{aligned}$$

32. (A)

Young modulus depends on material of wire not on length and area of wire's cross section.

33. (C)

(e) Force $F = YA \frac{\Delta l}{l}$ Y = young's modulus of the wire

$$= 2 \times 10^{11} \times 10^{-4} \left(\frac{2l - l}{l} \right) = 2 \times 10^7 \text{ N}$$

34. (D)

(d) Young's modulus,

$$Y = \frac{F/A}{\frac{\Delta l}{l}} = \frac{Fl}{A\Delta l} \Rightarrow \Delta l = \frac{Fl}{AY}$$

Net elongation, $\Delta l = \Delta l_1 + \Delta l_2$

$$\Rightarrow \Delta l = \frac{Fl_1}{A_1 Y_s} + \frac{Fl_2}{A_2 Y_c}$$

$$\Rightarrow F = \frac{\Delta l}{\frac{l_1}{A_1 Y_s} + \frac{l_2}{A_2 Y_c}} = \frac{\Delta l A}{\frac{l_1}{Y_s} + \frac{l_2}{Y_c}} \quad (\because A_1 = A_2 = A)$$

$$= \frac{1.4 \times 10^{-3} \times \pi \times (1.4 \times 10^{-3})^2}{\frac{3.2}{2 \times 10^{11}} + \frac{4.4}{1.1 \times 10^{11}}} = 1.54 \times 10^2 = 154 \text{ N}$$

35. (A)
 (a) Since breaking stress (Maximum lifting capacity) is the property of material so it will remain same.

$$\text{breaking stress} = \frac{\text{Maximum lifting capacity}}{\text{Area of cross-section of rope}}$$

$$\Rightarrow \frac{10}{2.5 \times 10^{-4}} = \frac{25}{A}$$

$$\Rightarrow A = \frac{25 \times 2.5 \times 10^{-4}}{10} = 625 \times 10^{-6} = 6.25 \times 10^{-4} \text{ m}^2$$

36. (C)
 (c) When length 'L' is hanging from fixed support

$$\Delta L = \frac{mgL}{\gamma A} \Rightarrow \Delta L \propto m$$

$$\Rightarrow \frac{\Delta L_1}{\Delta L_2} = \frac{m_1}{m_2} = \frac{1}{2} \Rightarrow \frac{L_1 - L}{L_2 - L} = \frac{1}{2}$$

$$\Rightarrow 2L_1 - 2L = L_2 - L \Rightarrow 2L_1 - L_2 = L$$

$$\therefore L = 2L_1 - L_2$$

37. (C)
 (c) At equilibrium, $\vec{F} = 0$

$$\Rightarrow \frac{-du}{dr} = 0 \Rightarrow \frac{-d}{dr} \left(\frac{A}{r^{10}} - \frac{B}{r^5} \right) = 0$$

$$\Rightarrow + \frac{A}{r^{11}} \times 10 - \frac{5B}{r^6} = 0 \Rightarrow \frac{1}{r^6} \left[\frac{10A}{r^5} - \frac{5B}{1} \right] = 0$$

$$\Rightarrow \frac{10A}{r^5} = 5B \Rightarrow r^5 = \frac{10A}{5B} \Rightarrow r = \left(\frac{2A}{B} \right)^{1/5}$$

38. (C)
 (c) Bulk modulus, $B = - \frac{\Delta P}{\frac{\Delta V}{V}} \Rightarrow \Delta P = -B \frac{\Delta V}{V}$

$$|\Delta P| = +3 \times 10^{10} \times 0.02 = 6 \times 10^8$$

39. (D)

(d) We know that terminal velocity is given by

$$V_T = \frac{2gr^2}{g\eta}(\rho - \rho_l)$$

Here, we have no involvement of buoyant force. So remove ρ_l .

$$\text{Then, } v_T = \frac{2gr^2\rho}{9\eta} = \frac{2 \times 10 \times 10^{-12} \times 10^3}{9 \times 1.8 \times 10^{-5}} = 123.4 \times 10^{-6} \text{ m/s.}$$

40. (A)

(a) As liquid drop is in equilibrium.

So $F_{\text{net}} = 0$

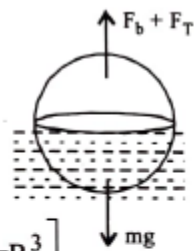
Boyant force + surface tension = mg

$$\sigma \frac{V}{2} g + 2\pi RT = \rho Vg$$

$$\Rightarrow 2\pi RT = \frac{(2\rho - \sigma)}{2} \frac{4}{3} \pi R^3 g \left[\because V = \frac{4}{3} \pi R^3 \right]$$

$$\Rightarrow R^3 = \frac{3T}{(2\rho - \sigma)g} \Rightarrow R = \sqrt{\frac{3 \times 7.5 \times 10^{-2} \text{ N-m}^{-1}}{(2\rho - \sigma) \times 10}}$$

$$\Rightarrow R = \frac{3}{20\sqrt{(2\rho - \sigma)}} \text{ m} = \frac{15}{\sqrt{2\rho - \sigma}} \text{ cm}$$



41. (A)

(a) $E_i = 0^- A_i 0^-$ = surface energy per unit area

$$= T a_i \left[\because 0^- = T \right] = T \cdot 4\pi r_i^2$$

$$\text{Now, } V_i = V_f \Rightarrow \frac{4}{3} \pi r_i^3 = 64 \times \frac{4}{3} \pi r_f^3 \Rightarrow r_i^3 = 64 r_f^3$$

$$\Rightarrow r_i = 4r_f$$

$$\text{So, } E_f = 0^- A_f = T \times 64 \times 4\pi r_f^2 = 256T \times \pi \frac{r_i^2}{16} = 16\pi T r_i^2$$

$$\text{So, } \Delta E = E_f - E_i = 12\pi + T r_i^2 = 12\pi \times 0.075 \times 0.1^2 = 2.82 \times 10^{-4} \text{ J}$$

42. (101)

(101) Given : Radius of capillary tube,

$$r = 0.015 \text{ cm} = 15 \times 10^{-5} \text{ mm}$$

$$h = 15 \text{ cm} = 15 \times 10^{-2} \text{ mm}$$

$$\text{Using, } h = \frac{2T \cos \theta}{\rho g r} \quad [\cos \theta = \cos 0^\circ = 1]$$

Surface tension,

$$T = \frac{r h \rho g}{2} = \frac{15 \times 10^{-5} \times 15 \times 10^{-2} \times 900 \times 10}{2} = 101$$

milli newton m^{-1}

43. (4)

$$\text{(4) } T = Ml\omega^2$$

$$\sigma = \frac{T}{A} = \frac{ml\omega^2}{A}$$

$$\frac{ml\omega^2}{A} \leq 48 \times 10^7 \Rightarrow \omega^2 \leq \frac{(48 \times 10^7) A}{ml}$$

$$\Rightarrow \omega^2 \leq \frac{(48 \times 10^7)(10^{-6})}{10 \times 3} = 16 \Rightarrow \omega_{\max} = 4 \text{ rad/s}$$

44. (40)

(40) Let m be mass that can be placed in the pan. For wire W_1

$$\text{Stress} = \frac{\text{Maximum weight}}{\text{Area}} = \frac{(m + 30)g}{8 \times 10^{-7}}$$

$$\Rightarrow m + 30 = 1.25 \times 10^9 \times 8 \times 10^{-7}$$

$$\Rightarrow m + 30 = 100 \Rightarrow m = 70 \text{ kg}$$

For wire W_2

$$\text{Stress} = \frac{(m + 10)g}{4 \times 10^{-7}} = 1.25 \times 10^9$$

$$\Rightarrow m + 10 = 50 \Rightarrow m = 40 \text{ kg}$$

Maximum mass that can be placed = 40 kg.

45. (20)

Energy stored in stretched catapult is converted into kinetic energy of stone

$$\frac{1}{2} \cdot \frac{YA}{L} \cdot x^2 = \frac{1}{2} mv^2$$

$$\frac{0.5 \times 10^9 \times 10^{-6} \times (0.04)^2}{0.1} = \frac{20}{1000} v^2 \Rightarrow v^2 = 400$$

$$\therefore v = 20 \text{ m/s}$$

46. (2)

$$\text{As } \Delta l = \frac{F \cdot l}{Y \cdot \pi r^2} \Rightarrow \Delta l \propto \frac{l}{r^2}$$

$$\Delta l_2 = \left(\frac{l_2}{l_1}\right) \left(\frac{r_1}{r_2}\right)^2 \Delta l_1 = (2) \left(\frac{1}{2}\right)^2 (0.04) \text{ m} = 2 \text{ cm}$$

47. (500)

(500) Bulk modulus, $B = -\frac{\Delta P}{\left(\frac{\Delta V}{V}\right)}$

$$\Rightarrow B = -\frac{V}{dV} (\rho g h) \Rightarrow h = -\frac{B \frac{\Delta V}{V}}{\rho g}$$

$$\therefore h = \frac{9.8 \times 10^8 \times 0.5}{100 \times 10^3 \times 9.8} = 500 \text{ m.}$$

48. (2)

(2) Excess pressure inside bigger bubble = $\frac{4T}{r_2}$

So, Excess pressure inside the smaller soap bubble

$$\Delta P_1 = \frac{4T}{r_1} + \frac{4T}{r_2}$$

The excess pressure inside the equivalent soap bubble.

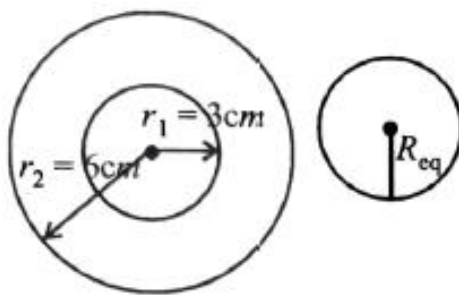
$$\Delta P_2 = \frac{4T}{R_{eq}}$$

$$\Delta P_1 = \Delta P_2$$

$$\Rightarrow \frac{4T}{R_{eq}} = \frac{4T}{r_1} + \frac{4T}{r_2}$$

$$\Rightarrow R_{eq} = \frac{r_1 r_2}{r_1 + r_2}$$

Putting $r_1 = 3 \text{ cm}$, $r_2 = 6 \text{ cm} \Rightarrow R_{eq} = 2 \text{ cm}$



49. (50)

(50) Given, length of metal wire, $\ell = 0.5 \text{ m}$

Cross-sectional area, $A = 10^{-4} \text{ m}^2$

Breaking stress $= 5 \times 10^8 \text{ Nm}^{-2}$

Mass of block $m = 10 \text{ kg}$

$T_{\text{max}} = \text{Breaking stress} \times \text{Area}$

$$\frac{mv^2}{\ell} = 5 \times 10^8 \times 10^{-4} = 5 \times 10^4$$

$$\frac{10 v^2}{0.5} = 5 \times 10^4 \Rightarrow v = \sqrt{\frac{0.5 \times 5 \times 10^4}{10}} = 50 \text{ m/s}$$

50. (30)

(30) Strain $= F/A Y = \frac{mg + \frac{mv^2}{R}}{A Y}$



$$= \frac{20 + \frac{2(5)^2}{0.5}}{3 \times 10^{-6} \times 10^{11}} = 30 \times 10^{-5}$$

51. (2)

(2) Slope $= \frac{\text{Extension/Load}}{\text{Length of wire}} = \frac{\Delta l/w}{L}$

Young's modulus, $Y = \frac{mg/A}{\Delta \ell/L} = \frac{wL}{\Delta \ell A}$

$$\therefore Y = \frac{1}{(\text{slope}) A} \Rightarrow Y = \frac{1}{2 \times 10^{-6} (0.25 \times 10^{-5})}$$

$$\Rightarrow Y = 2 \times 10^{11} \text{ N/m}^2$$

52. (25)

Given mass of rod $m = 20 \text{ kg}$

Cross-section area, $A = 0.4 \text{ m}^2$

Length $\ell = 20 \text{ m}$

Let extension is dy in length dx .

$$Y = \frac{\text{stress}}{\text{strain}} = \frac{\frac{T}{A}}{\frac{dy}{dx}} = \frac{T}{A} \cdot \frac{dx}{dy} \Rightarrow dy = \frac{T dx}{A Y}$$

Tension at a distance x from lower end $T = \frac{mg}{\ell} x$

$$\int_0^{\Delta \ell} dy = \int_0^{\ell} \frac{mg}{\ell} x \frac{dx}{A Y} \Rightarrow \Delta \ell = \frac{mg}{\ell A Y} \left[\frac{x^2}{2} \right]_0^{\ell}$$

$$\Delta l = \frac{mg\ell}{2AY} = \frac{20 \times 10 \times 20}{2 \times 0.4 \times 2 \times 10^{11}} = 25 \times 10^{-9} \text{ m}$$

Compare with $x \times 10^{-9}$ we have, $x = 25$

53. (5)

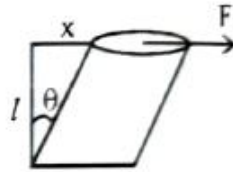
$$(5) \quad \Delta l = \frac{F\ell}{\gamma A} \Rightarrow \Delta l \propto \frac{F\ell}{r^2}$$

$$\Rightarrow \Delta l_2 = \Delta l_1 \left(\frac{F_2}{F_1} \right) \left(\frac{\ell_2}{\ell_1} \right) \left(\frac{r_1}{r_2} \right)^2 = 5 \times 4 \times 4 \times \frac{1}{16} = 5 \text{ cm}$$

54. (48)

$$(48) \quad \eta = \frac{F}{A \tan \theta} = \frac{F}{A \left(\frac{x}{\ell} \right)}$$

$$\frac{F}{A} = \eta \frac{x}{\ell} \Rightarrow \frac{F\ell}{A\eta} = x$$



$$\Rightarrow x = \frac{18 \times 10^4 \times 60 \times 10^{-2}}{60 \times 10^{-2} \times 15 \times 10^{-2} \times 25 \times 10^2} = 48 \times 10^{-6} \text{ m} = 48 \mu \text{ m}$$

55. (25)

$$(25) \quad y = \frac{\text{stress}}{\text{strain}} \Rightarrow \text{strain} = \frac{1}{y} \text{ stress}$$

$$\therefore \frac{1}{y} = \text{slope} = \frac{(2-1) \times 10^{-10}}{40-20} = \frac{1}{20} \times 10^{-10} \Rightarrow y = 20 \times 10^{10}$$

$$\text{So, energy density} = \frac{1}{2} \times \text{stress} \times \text{strain}$$

$$= \frac{1}{2} \times y \times (\text{strain})^2 = \frac{1}{2} \times 20 \times 10^{10} \times (5 \times 10^{-4})^2$$

$$= 10^{11} \times 25 \times 10^{-8} = 25 \times 10^3 = 25 \text{ kJ/m}^3$$

56. (25)

$$(25) \quad F_V + F_B = mg \quad (V = \text{constant})$$

$$F_V = mg - F_B = \rho_B Vg - \rho_L Vg = (\rho_B - \rho_L)Vg$$

$$= (8 - 1.3) \times 10^{+3} \times \frac{0.3 \times 10^{-3}}{8 \times 10^3} \times 10 = 25 \times 10^{-4} \text{ N}$$

Hence, the value of viscous force acting on ball will be $25 \times 10^{-4} \text{ N}$.

Compare with $x \times 10^{-4}$, we get $x = 25$

57. (11)

(11) When bubble is rising steadily the net force acting on it will be zero.

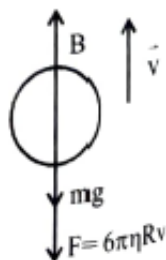
So, buoyant force (B) = drag force (F)

$$\Rightarrow \frac{4\pi}{3}R^3\rho g = 6\pi\eta Rv$$

$$\therefore \eta = \frac{4}{18} \frac{R^2\rho g}{v}$$

$$\text{or, } \eta = \frac{4}{18} \frac{(10^{-3})^2 \times 1.75 \times 10^3 \times 10}{0.35 \times 10^{-2}}$$

$$\therefore \eta = \frac{10}{9} = 1.11 = 11 \text{ poise}$$



58. (20)

(20) Speed after falling 'h' height = Terminal velocity

$$\Rightarrow \sqrt{2gh} = \frac{2r^2g}{g\eta}(\rho - \rho_f)$$

$$\Rightarrow \sqrt{2 \times 10 \times h} = \frac{2 \times (0.1 \times 10^{-3})^2 \times 10}{9 \times 10^{-5}} \times (10^4 - 10^3)$$

$$\Rightarrow \sqrt{20h} = \frac{2 \times 10^{-8} \times 10}{9 \times 10^{-5}} \times 9 \times 10^3$$

$$\Rightarrow \sqrt{20h} = 20 \Rightarrow 20h = 400 \Rightarrow h = 20 \text{ m}$$

59. (500)

$$(500) P = P_0 + \frac{2T}{R} \Rightarrow P - P_0 = \frac{2T}{R}$$

$$500 = \frac{2 \times T}{2 \times 10^{-3}}$$

$$T = 500 \times 10^{-3}$$

$$\text{So, } x = 500$$